

East-of-Hudson Stormwater Retrofit Plan (Years 6 – 10)

# FAD and Connected Basin Phosphorus Reduction - 391 KG

Prepared for: East of Hudson Coalition & Pamela L. Young, Ph.D. Chief, NYC Watershed Section Bureau of Water Supply Protection NYS Department of Health Corning Tower Rm. 1198 Empire State Plaza Albany, NY 12237

September 14, 2016

# Prepared by:





A ENGINEERING DESIGN



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## 1. INTRODUCTION & PURPOSE

The East of Hudson Coalition (EOHC) consists of 19 municipal entities located within the East of Hudson Watershed, who are required to reduce the levels of phosphorus that discharge into the East of Hudson Watershed via stormwater runoff, in order to comply with their NYSDEC MS4 General Permit requirements. These permitting requirements have been developed to protect the water quality of the East of Hudson Watershed, which supplies drinking water to New York City, and parts of Westchester and Putnam Counties.

The EOHC consists of the following 19 municipal entities: Bedford, Brewster, Carmel, Cortlandt, Kent, Lewisboro, Mount Kisco, New Castle, North Castle, North Salem, Patterson, Pound Ridge, Putnam County, Putnam Valley Somers, Southeast, Town of Pawling, Village of Pawling, and Yorktown. Phosphorus reduction is achieved via the construction of NYSDEC approved Stormwater Retrofit Practices (SRPs) that collect and treat stormwater runoff.

The initial MS4 General Permit required the EOHC municipal entities to collectively reduce phosphorus by 459.5 kg/year, over a 5-year implementation period (i.e. Years 1-5). Stormwater retrofit plans for Years 1-5 of the program were completed, and consisted of identifying potential stormwater retrofit projects to achieve a phosphorus reduction of 459.5 kg/year. The results of the Years 1-5 stormwater retrofit plans continue to be implemented and administered by the East of Hudson Watershed Corporation (EOHWC).

Woodard & Curran, in conjunction with its partners Paggi Engineering and Rennia Engineering, was contracted by the EOHC to develop a new stormwater retrofit plan. This plan consists of identifying stormwater retrofit projects within the Filtration Avoidance Determination (FAD) basins, including those basins that are hydrologically connected to the FAD basins, over a new 5-year implementation period; Years 6-10.

The Stormwater Retrofit Plan (Years 6-10), located in Appendix A, identifies 86 projects with the potential to achieve a phosphorus reduction of 391 kg/year, and includes estimated design/construction costs. Corresponding project plans titled "Stormwater Retrofit Concept Plans" and calculations for each individual project are located in Appendix B. All calculations and removal efficiencies have been performed in accordance with the latest NYSDEC approved design parameters and calculations, which are also captured in the latest version of the EOHWC Design Manual.

The remaining sections of the report narrative discuss the process implemented to develop the Stormwater Retrofit Plan (Years 6-10), and conclusions/recommendations to assist in the implementation of the proposed conceptual stormwater retrofit projects during Years 6 - 10 of the NYSDEC MS4 program.



## 2. PLAN DEVELOPMENT & PROCESS

The goal of the EOHC and the Woodard & Curran team was to generate a successful Stormwater Retrofit Plan for Years 6-10 that took into account the experience gained and lessons learned from the development, administration, and implementation of the stormwater retrofit plans in Years 1-5 of the program.

Based on feedback from the EOHC and municipal staff, as well as our team's experience involved in the feasibility, design, permitting, and construction oversight of numerous Years 1-5 stormwater retrofit projects, our goal was to develop a plan and identify stormwater retrofit projects using the following criteria:

- Identify sites that contain a high density of impervious surfaces in order to focus on high phosphorus loading opportunities; focus on sites with a minimum of 3.5 acres of impervious surfaces; avoid large watershed areas that are exclusively wooded or developed open space.
- Consider sites and practices that rely on natural runoff pathways (sheet, open channel flow) or existing pipe networks to collect and convey runoff to proposed SRPs. Based on our experience, projects that require the design and construction of runoff collection and conveyance infrastructure significantly increases the overall SRP cost.
- Ensure accessibility to the project site and the SRP; confirm that any new SRP would not interfere with existing site operations.
- Consider sites that contain eroded channels or outfall locations with ongoing erosion or the potential for erosion (on both public and private property).
- Identify any recently designed/constructed stormwater improvement projects that may qualify for eligible phosphorus reduction credits as part of the EOHC MS4 program.
- Consider public/private partnerships with commercial landowners with large areas of existing impervious surfaces (i.e. corporate parks, large corporations, & retail centers) that are in good standing with the Town/Village.
- Focus on the more cost effective SRPs constructed in Years 1-5 such as water quality ponds, surface sand filters, and channel stabilization projects. Calculate any potential channel stabilization phosphorus credits using the NYSDEC approved revised channel stabilization calculation methodology.
- Consider the logistics and magnitude of SRP operations and maintenance with the understanding that long-term cost is a major concern for the municipalities.
- Use the above criteria to generate a list of projects to maximize the phosphorus reduction goal.



The Woodard & Curran team took into consideration the above-mentioned criteria, and developed the Stormwater Retrofit Plan (Years 6-10) by implementing the following process to identify applicable project sites and SRPs:

- We obtained and reviewed historical records related to Years 1 5, to ensure we did not duplicate efforts, and to determine if there remained any potential feasible projects.
- The latest version of the NYCDEP GIS database was obtained and customized to include additional data layers related to environmental features such as wetlands and floodplains, and we added other features to more efficiently identify and measure impervious areas.
- Standardized calculation worksheets were developed based upon NYSDEC feedback regarding calculation methodology and input parameter updates. Such updates included the confirmation that the actual calculated Rv is to be used in the water quality volume calculations (i.e. a minimum Rv of 0.2 is not applicable), and the EMC value for open developed space has been reduced by 50%.
- Upon updating and customizing the GIS database, we completed a desktop analysis to identify applicable project sites that met the SRP qualification criteria noted on the previous page. We created maps of all potential project sites for future discussions with the 19 EOHC municipal entities.
- A standard agenda was developed prior to meeting with each municipal entity that included the SRP selection criteria. The agenda and potential project sites maps were sent to each municipal entity, and a meeting was scheduled and conducted with municipal staff. The agenda and initially identified project sites were discussed, and revised project lists were developed based upon municipal staff input. We also met separately with large private commercial property owners such as IBM in Somers, as noted on the Stormwater Retrofit Concept Plans located in Appendix B. We discussed the likelihood of gaining future approvals from private homeowners for proposed channel stabilization projects that were located entirely or partially within private lots. We only included those in which the Towns were confident that private homeowners would not oppose the project.
- The Woodard & Curran team conducted site visits to further assess the proposed SRP feasibility. A revised SRP list was developed including proposed phosphorus reduction values and design/construction cost estimates, and distributed to each municipal entity for a last round of input.
- Once the SRP list was finalized, all Stormwater Retrofit Concept Plans were developed and the Stormwater Retrofit Plan (Years 6-10) was finalized. Multiple SRPs are proposed for certain project sites to allow for flexibility with the regulatory approval process, in the event that future subsurface site investigations result in the determination that the primary SRP is infeasible.
- During this overall process, we submitted a request to the NYSDEC to expand the currently approved SRP list to include the StormBasin with FABPHOS catch basin filter proprietary product, manufactured by FABCO. This SRP is a product that can be inserted into existing catch basins to treat phosphorus. Refer to Appendix C for a complete version of the submittal including product details and specifications, and a copy of the subsequent NYSDEC approval. This approved product provides the EOHC with an additional SRP option for sites where traditional practices identified in the Stormwater Retrofit Plan (Years 6-10) are not feasible.



## 3. CONCLUSION & RECOMMENDATIONS

Based upon the due diligence described in the previous report sections, the Stormwater Retrofit Plan (Years 6-10) located in Appendix A achieves the following objectives:

- The lessons learned and valuable experience gained from Years 1 through 5 of the program have been factored into the preparation of the plan, maximizing the likelihood of implementing feasible and cost effective SRPs.
- The proposed SRP's are highly focused to obtain the best phosphorus removal and the best cost.

In conclusion, we offer the following recommendations to further improve the implementation of the Stormwater Retrofit Plan (Years 6-10):

- Consider first implementing the design and construction of all channel stabilization projects as they
  have the greatest variability in the final potential phosphorus reduction values, due to the involved
  nature of the calculation methodology. The selection and implementation of the remaining SRPs
  included in the Stormwater Retrofit Plan (Years 6-10) can be re-evaluated once the phosphorus
  figures for the channel stabilization projects have been finalized.
- Next, consider implementing those practices that fit within the footprint of municipally owned or controlled properties and which do not require advanced permitting with state and federal agencies.
- Then work with the identified private landowners to continue the implementation of public/private partnership projects that have the potential for large phosphorus reductions.
- We recommend that the EOHC work closely with the EOHWC to ensure communications are maintained between the municipal entities and any private property owners during the Years 6 10 implementation process on a continuous basis to keep key or new points of contact up to date.
- Lastly, in order to streamline the overall implementation process and minimize change orders during the engineering design phase, we first recommend completing the "Initial Evaluation" (as referenced in the latest version of the EOHWC Design Manual) prior to engaging in contracts for 100% design/bid documents. Completing the Initial Evaluation (this process includes subsurface field investigations including deep holes and percolation testing) up front will result in the determination of the feasibility of all SRPs. By determining the feasibility of all SRPs prior to engaging in the final design process, EOHC can minimize the potential for change orders during the design process and investing too much time and resources in projects that may ultimately fail.



# APPENDIX A: STORMWATER RETROFIT PLAN (YEARS 6 – 10)



## East of Hudson Coalition Years 6 - 10 Project List

August 12, 2016

Revised: September 2, 2016 (remove all non-FAD Basin projects)

#### **General Notes:**

- A. This project list represents the Phase 1 level of vetting as included in our proposal. It was developed based on GIS desktop reviews of the NYCDEP, EOHWC, and W&C databases and customized layers, meetings with Town representatives and initial discussions with property owners, and site visits to confirm SRP compatibility with the property constraints and operations.
- B. This list has been developed with the review and input of the host municipalities.
- C. The cost data reflected in this table is based on a compilation and analysis of EOHWC records to date for projects in Years 1-5, in which accurate cost data exists for design and constructions costs (a function of construction bids or EOPCCs based on 100% design documents in the absence of construction bids). The cost data included in the table accounts for a 15% contingency due to the preliminary and conceptual nature of the SRP identification process and design/calculations, as well as having less opportunity for projects on public lands. The costs also reflect 5 years of inflation at 3% per year.
- D. The column titled "Estimated Project Cost (Design + Construction)" is a function of the weighted average cost per Kg per SRP (design and construction) as calculated in Table 2 listed at the bottom of this document, based on EOHWC records. The table also includes the lowest and highest design and construction costs per SRP encountered in Year 1-5, to provide a comprehensive view of potential expected costs in Years 6-10.
- E. Channel stabilization projects presented in this table do not account for any potential additional phosphorus removal credits associated with proposed design/construction of upgradient SRP's, unless noted otherwise on the conceptual project plan. The removal credits presented in the table have been calculated under the latest NYSDEC approved BANCS method equations, and assume a soil loss depth of 0.065.
- F. The SRPs presented in this table are the primary proposed SRPs for each project, intended to maximize phosphorus removal and cost efficiency. Consistent with the approach included in our initial project approach, Conceptual Project Plans may include secondary and tertiary proposed SRP options. These secondary/tertiary options (as applicable) will only be included in the Conceptual Project Plans, and are intended to provide flexibility during the regulatory review phase in the event that the primary SRP is deemed infeasible.

#### Summar

\*FAD Basi (not including hydrologically cor (kg/yr) / # of pro estimated pr

FAD Basin (including u hydrologically cor (kg/yr) / # of total estimated

\*Only includes valu and West Branch.

	Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
1	VB-1, Putnam Terrace	Public	19 Putnam Terrace	Putnam	Brewster	Surface Sand Filter	Diverting	Yes	-	0.78	\$52,380	\$31,586 - \$113,133
2	VB-2, Railroad Ave (Commuter Parking Lot)	Public	390 Railroad Ave (Park Street)	Putnam	Brewster	Surface Sand Filter	Diverting	Yes	-	2.08	\$139,680	\$84,229 - \$301,689
3	VB-3, Southeast Museum/Brewster Library (Rear Parking Lot)	Public	67/79 Main Street	Putnam	Brewster	Surface Sand Filter	Diverting	Yes	-	1.05	\$70,511	\$42,520 - \$152,295
4	Carmel-1A, Arborview Rd - A	Public	Arborview Rd	Putnam	Carmel	Wet Extended Detention Pond <sup>3</sup>	Croton Falls	Yes	-	7.28	\$891,969	\$305,849 - \$2,097,931
5	Carmel-1B, Arborview Rd - B	Public	Arborview Rd	Putnam	Carmel	Wet Extended Detention Pond <sup>3</sup>	Croton Falls	Yes	-	4.24	\$519,499	\$178,132 - \$1,221,872



#### RENNIA ENGINEERING DESIGN, PLLC CML + ENVIRONMENTAL + STRUCTURAL

6Dover Wage Plaza, Suite 5: P.O. Box 400, Dover Plaza, Nr 12522 Tat (\$45) 577-055 Fac: (\$45) 877-0556

y of Proposed Year 6-10 Phosphorus Reduction									
in Total g upstream nnected basins) rojects / total roject cost	*74.14 / 20 / \$7,023,627								
n Total upstream nnected basins) f projects / d project cost	391.35 / 86 / \$36,646,028								

\*Only includes values for the following drainage basins: Cross River, Croton Falls, Boyd Corners

Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
6 Carmel-2, Eleanor Drive - A	Public	14 Eleanor Dr	Putnam	Carmel	Channel Stabilization	Croton Falls	Yes	-	4.22	\$184,108	\$42,585 - \$289,851
7 Carmel-4A, Putnam Hospital Center	- A Private	670 Stoneleigh Ave	Putnam	Carmel	Wet Extended Detention Pond <sup>3</sup>	Croton Falls	Yes	-	4.14	\$507,246	\$173,931 - \$1,193,054
8 Carmel-4B, Putnam Hospital Center	- B Private	670 Stoneleigh Ave	Putnam	Carmel	Wet Extended Detention Pond <sup>3</sup>	Croton Falls	Yes	No	6.21	\$760,870	\$260,896 - \$1,789,582
9 Carmel-5A, Putnam Plaza - A	Private	1906 US-6	Putnam	Carmel	Proprietary Filtering Practices	Croton Falls	Yes	No	0.93	\$67,244	\$48,037 - \$228,073
10 Carmel-5B, Putnam Plaza - B	Private	1906 US-6	Putnam	Carmel	Proprietary Filtering Practices	Croton Falls	Yes	-	0.41	\$29,645	\$21,178 - \$100,548
11 Carmel-5C, Putnam Plaza - C	Private	1906 US-6	Putnam	Carmel	Proprietary Filtering Practices	Croton Falls	Yes	-	1.32	\$95,443	\$68,182 - \$323,717
12 Carmel-5D, Putnam Plaza - D	Private	1906 US-6	Putnam	Carmel	Proprietary Filtering Practices	Croton Falls	Yes	-	1.01	\$73,028	\$52,170 - \$247,692
13 Carmel-7, Tanya Lane	Public	Tanya Lane	Putnam	Carmel	Wet Extended Detention Pond	Croton Falls	Yes	No	5.41	\$662,851	\$227,286 - \$1,559,040
14 Carmel-9A, Willow Road East	Private	Willow Rd	Putnam	Carmel	Channel Stabilization	Lake Gleneida	Yes	-	8.00	\$349,019	\$80,730 - \$549,480
15 Carmel-9B, Willow Road West	Private	Willow Rd	Putnam	Carmel	Channel Stabilization	Lake Gleneida	Yes	-	5.88	\$256,529	\$59,336 - \$403,868
16 Kent-1, Kent Highway Garage	Public	62 Ludington Rd	Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	1.82	\$122,220	\$73,700 - \$263,978
17 Kent-2, Montrose Drive Outfall	Public	Montrose Dr & Greenridge Ct	e Putnam	Kent	Multiple Pond System	Middle Branch	Yes	-	20.50	\$2,511,727	\$861,252 - \$5,907,637
18 Kent-3, Chuang Yen Monastery	Private	2020 Rt 301	Putnam	Kent	Surface Sand Filter	Boyd Corners	Yes	-	3.05	\$204,819	\$123,509 - \$442,380
19 Kent-4, Lakeview Restaurant	Private	47 Route 311	Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	0.54	\$39,045	\$27,893 - \$132,430
20 Kent-5A, Lake Carmel - A	Public	Lakeshore Dr E & Lakeshore Dr S	Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	10.18	\$1,247,287	\$427,685 - \$2,933,646
21 Kent-5B, Lake Carmel - B	Public	Lakeshore Dr E & Harrima Rd	n Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	0.86	\$62,182	\$44,422 - \$210,906
22 Kent-5C, Lake Carmel - C	Public	Lakeshore Dr E & Harrima Rd	n Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	2.45	\$177,147	\$126,550 - \$600,838

Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
23 Kent-5D, Lake Carmel - D	Public	Lakeshore Dr E & Caryl Rd	Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	1.09	\$78,812	\$56,302 - \$267,311
24 Kent-5E, Lake Carmel - E	Public	Lakeshore Dr E & Hawthorne Rd	Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	2.50	\$180,762	\$129,133 - \$613,100
25 Kent-5F, Lake Carmel - F	Public	Lakeshore Dr E & Lockwood Rd	Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	1.75	\$214,416	\$73,521 - \$504,310
26 Kent-5G, Lake Carmel - G	Public	Lakeshore Dr E & Stanwich Rd	Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	2.00	\$245,047	\$84,025 - \$576,355
27 Kent-5H, Lake Carmel - H	Public	Lakeshore Dr E & Huguenc Rd	t Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	2.31	\$283,029	\$97,048 - \$665,690
28 Kent-5I,Lake Carmel - I	Public	Lakeshore Dr E & Yorktow Rd	<sup>n</sup> Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	2.23	\$273,227	\$93,687 - \$642,636
29 Kent-5J, Lake Carmel - J	Public	Lakeshore Dr E & Clubhouse Dr	Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	4.26	\$521,949	\$178,972 - \$1,227,636
30 Kent-5K, Lake Carmel - K	Public	Lakeshore Dr E & Woodland Dr	Putnam	Kent	Wet Extended Detention Pond	Middle Branch	Yes	-	4.39	\$537,877	\$184,434 - \$1,265,099
31 Kent-5L, Lake Carmel - L	Public	Lakeshore Dr E & Fleetwood Rd	Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	1.63	\$117,857	\$84,195 - \$399,741
32 Kent-5M, Lake Carmel - M	Public	Lakeshore Dr E & Placid Rc	l Putnam	Kent	Proprietary Filtering Practices	Middle Branch	Yes	-	2.44	\$176,424	\$126,034 - \$598,385
33 Kent-6A, Kent Elementary School - A	School	1065 Rt 52	Putnam	Kent	Subsurface Infiltration	West Branch	Yes	-	4.75	\$755,117	\$296,884 - \$1,714,293
34 Kent-6B, Kent Elementary School - B	School	1065 Rt 52	Putnam	Kent	Surface Sand Filter	West Branch	Yes	-	2.86	\$192,060	\$115,815 - \$414,822
35 Kent-6C, Kent Primary School	School	1065 Rt 52	Putnam	Kent	Surface Sand Filter	Middle Branch	Yes	-	4.21	\$282,717	\$170,483 - \$610,630
36 L-4, Lewisboro Elementary School	School	79 Bouton Rd	Westchester	Lewisboro	Surface Sand Filter	Cross River	Yes	-	2.64	\$177,286	\$106,906 - \$382,913
37 L-5, Lewisboro Town Park	Public	890 Rt 35	Westchester	Lewisboro	Subsurface Infiltration	Cross River	Yes	-	3.00	\$476,916	\$187,506 - \$1,082,711
38 L-6, Long Pond Preserve	Private	Mead St & Tarry A Bit Dr	Westchester	Lewisboro	Channel Stabilization	Cross River	Yes	Class "C" 4	14.62	\$956,749	-
39 Pat-1, Big Elm Detention Pond	Private	1 Bradley Dr	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	2.71	\$332,038	\$113,853 - \$780,961

Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
40 Pat-10A, Robin Hill Corporate Park - A	Private	20 Jon Barrett Road	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	6.94	\$850,312	\$291,565 - \$1,999,951
41 Pat-10B, Robin Hill Corporate Park - B	Private	40 Jon Barrett Road	Putnam	Patterson	Pocket Pond <sup>3</sup>	East Branch	Yes	-	2.12	\$259,749	\$89,066 - \$610,936
42 Pat-10C, Robin Hill Corporate Park - C	Private	50 Jon Barrett Road	Putnam	Patterson	Pocket Pond <sup>3</sup>	East Branch	Yes	-	2.26	\$276,903	\$94,948 - \$651,281
43 Pat-10D, Robin Hill Corporate Park - D	Private	60 Jon Barrett Road	Putnam	Patterson	Pocket Pond <sup>3</sup>	East Branch	Yes	-	3.72	\$455,787	\$156,286 - \$1,072,020
44 Pat-10E, Robin Hill Corporate Park - E	Private	70 Jon Barrett Road	Putnam	Patterson	Pocket Pond <sup>3</sup>	East Branch	Yes	-	2.48	\$303,858	\$104,190 - \$714,680
Pat-11A, Watchtower Education Center 45 - A	<sup>er</sup> Private	100 Watchtower Dr	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	6.09	\$746,167	\$255,855 - \$1,755,000
Pat-11B, Watchtower Education Center - B	er Private	100 Watchtower Dr	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	3.16	\$387,174	\$132,759 - \$910,641
47 Pat-12B, CT Stream - B	Private	Valley Road	Putnam	Patterson	Multiple Pond System	East Branch	Yes	Class "C" 4	19.80	\$2,425,961	\$831,843 - \$5,705,913
48 Pat-13, Dayton Road	Public	15 Dayton Road	Putnam	Patterson	Channel Stabilization	East Branch	Yes	-	11.63	\$1,424,946	\$488,603 - \$3,351,503
49 Pat-2, Clancy Relocation & Logistics	Private	2963 Rt 22	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	No	4.14	\$507,246	\$173,931 - \$1,193,054
50 Pat-3, Devon Road	Private	Devon Rd & Cornwall Hill Rd	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	No	2.70	\$330,813	\$113,433 - \$778,079
51 Pat-4, Fox Run Condominiums	Private	Fox Run Ln	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	Middle Branch	Yes	-	6.28	\$769,446	\$263,837 - \$1,809,754
<sup>52</sup> Pat-5, Gottwald Property <sup>1</sup>	Public/Private	384 Fair Street	Putnam	Patterson	Pocket Pond	Middle Branch	Yes	-	5.92	\$725,338	\$248,713 - \$1,706,010
53 Pat-6, Indian Hill Road	Private	16 Indian Hill Road	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	5.71	\$699,608	\$239,890 - \$1,645,493
54 Pat-7, JRS Pharma	Private	2981 Rt 22	Putnam	Patterson	Subsurface Infiltration	East Branch	Yes	-	6.02	\$957,012	\$376,262 - \$2,172,641
55 Pat-8A, Manor Road - A	Private	21 Manor Rd	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	1.22	\$149,478	\$51,255 - \$351,576
56 Pat-8B, Manor Road - B	Private	14 Kings Way	Putnam	Patterson	Wet Extended Detention Pond <sup>3</sup>	East Branch	Yes	-	3.60	\$441,084	\$151,244 - \$1,037,439

Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
57 Pat-9A, Putnam Lake - A	Private	Lake Shore Dr & Jackson R	Rd Putnam	Patterson	Proprietary Filtering Practices	East Branch	Yes	-	1.16	\$83,874	\$59,918 - \$284,478
58 Pat-9B, Putnam Lake - B	Private	Lake Shore Dr & Dayton R	d Putnam	Patterson	Proprietary Filtering Practices	East Branch	Yes	-	5.23	\$378,155	\$270,146 - \$1,282,604
59 Pat-9C/D, Putnam Lake - C/D	Private	Lake Shore Dr & Fulton Dr	· Putnam	Patterson	Proprietary Filtering Practices	East Branch	Yes	-	13.81	\$998,532	\$713,331 - \$3,386,762
<sup>60</sup> Pat-12A, CT Stream - A <sup>2</sup>	Private	Purdum Rd	New Fairfield	Patterson	Channel Stabilization	East Branch	Yes	Class "C" <sup>4</sup>	25.13	\$1,096,356	\$253,592 - \$1,726,054
61 PR-1, Ambler Way	Private	Ambler Way & Boutonville Road	e Westchester	Pound Ridge	Channel Stabilization	Cross River	Yes	No	0.25	\$10,907	\$2,523 - \$17,171
62 PR-3, Parkview Drive	Private	114 Parkview Drive	Westchester	Pound Ridge	Channel Stabilization	Cross River	Yes	No	1.39	\$60,642	\$14,027 - \$95,472
63 PR-4, Dingee Road	Private	26 Dingee Road	Westchester	Pound Ridge / Lewisboro	Channel Stabilization	Cross River	Yes	No	2.31	\$100,779	\$23,311 - \$158,662
64 PC-2, Putnam County Sheriff's Facility	Public	3 County Center & 40 Gleneida Avenue	Putnam	Putnam County	Stormfilter	Cross River	Yes	-	4.10	\$296,450	\$211,778 - \$1,005,483
65 PC-1_Stagecoach Road	Public	Stagecoach Road	Putnam	Putnam County	Channel Stabilization	East Branch	Yes	No	2.25	\$98,162	\$22,705 - \$154,541
66 SE-11, Highview Terrace - Channel	Public / Private	33 Highview Terrace	Putnam	Southeast	Channel Stabilization	Diverting	Yes	No	1.74	\$75,912	\$17,559 - \$119,512
67 SE-12, Federal Hill Road - Channel	Private	118-120 Federal Hill Rd	Putnam	Southeast	Channel Stabilization	East Branch	Yes	No	2.64	\$115,176	\$26,641 - \$181,328
SE-1A, Upper Brewster Hill Road - Channel	Private	Brewster Hill Road	Putnam	Southeast	Channel Stabilization	Diverting	Yes	Class "C" <sup>4</sup>	9.77	\$639,359	-
69 SE-1B, Lower Brewster Hill Road - Channel	Public / Private	Brewster Hill Road	Putnam	Southeast	Channel Stabilization	Diverting	Yes	Class "C" <sup>4</sup>	21.95	\$1,436,432	-
70 SE-2, Eagles Ridge	Private	304 Eagles Ridge Road	Putnam	Southeast	Surface Sand Filter	Diverting	Yes	-	5.54	\$372,032	\$224,341 - \$803,537
5E-3, Garden Homes Brewster (Upgrade Existing Detention Facility)	Private	1618-1624 Rt 22	Putnam	Southeast	Pocket Pond	Bog Brook	Yes	-	4.69	\$574,634	\$197,038 - \$1,351,552
72 SE-4, Lake Tonetta	Public	140 Pumphouse Road	Putnam	Southeast	Subsurface Infiltration	Diverting	Yes	-	1.83	\$290,919	\$114,379 - \$660,454
SE-5, Midtown Trackage Ventures LLC (MTA Parking Lot)	Private	Independent Way	Putnam	Southeast	Surface Sand Filter	Diverting	Yes	-	5.69	\$382,105	\$230,415 - \$825,293

Project Name	Ownership	Site Address	County	Municipality	Proposed Retrofit	Reservoir	FAD Basin?	Classified Stream?	Estimated Phosphorus Reduction (kg/yr)	Estimated Project Cost (Design + Construction)	Historical Project Cost Range (Design + Construction)
74 SE-6, Mount Kisco Medical Group	Private	185 NY-312	Putnam	Southeast	Surface Sand Filter	Middle Branch	Yes	-	2.35	\$157,811	\$95,163 - \$340,850
75 SE-7, Powers Products III LLC	Private	2 Powers Lane	Putnam	Southeast	Surface Sand Filter	Bog Brook	Yes	-	3.71	\$249,141	\$150,236 - \$538,109
76 SE-8, Scolpino Park	Public	Doansburg Rd	Putnam	Southeast	Surface Sand Filter	East Branch	Yes	-	1.34	\$89,986	\$54,263 - \$194,357
77 SE-10, 16 Mt. Ebo Road South	Private	16 Mt. Ebo Road South	Putnam	Southeast	Surface Sand Filter	East Branch	Yes	-	1.58	\$106,103	\$63,982 - \$229,168
78 SE-9, 15 Mt. Ebo Road South	Private	15 Mt. Ebo Road South	Putnam	Southeast	Surface Sand Filter	Bog Brook	Yes	-	3.39	\$227,651	\$137,277 - \$491,695
79 PW-1, 158 Route 22 LLC	Private	158 Route 22	Dutchess	Town of Pawling	Pocket Pond	East Branch	Yes	-	6.16	\$754,743	\$258,796 - \$1,775,173
80 PW-2, Daley, John	Private	3874 Route 55	Dutchess	Town of Pawling	Channel Stabilization	East Branch	Yes	No	3.00	\$130,882	\$30,274 - \$206,055
81 PW-3, Pawling Fire Dept Inc.	Public	25 South Street	Dutchess	Town of Pawling	Proprietary Filtering Practices	East Branch	Yes	-	1.87	\$135,210	\$96,591 - \$458,599
82 PW-4, South Street	Public	53 South Street	Dutchess	Town of Pawling	Multiple Pond	East Branch	Yes	-	3.77	\$461,913	\$158,386 - \$1,086,429
83 VPW-1, Mizzentop Day School	Private	535 Route 22	Dutchess	Village of Pawling	Pocket Pond	East Branch	Yes	-	2.55	\$312,434	\$107,131 - \$734,852
84 VPW-2, Lappas Inc.	Private	63 East Main Street	Dutchess	Village of Pawling	Proprietary Filtering Practices	East Branch	Yes	-	1.84	\$133,041	\$95,042 - \$451,241
85 VPW-3, Saint John's Church	Private	39 E Main St	Dutchess	Village of Pawling	Surface Sand Filter	East Branch	Yes	-	1.13	\$75,884	\$45,759 - \$163,898
86 VPW-4, Fairway Drive	Public	45 Fairway Dr	Dutchess	Village of Pawling	Proprietary Filtering Practices	East Branch	Yes	-	3.64	\$263,190	\$188,018 - \$892,673
-											

TOTALS:

ESTIMATED UNIT COST

391.35	\$36,646,028

\$98,694 per kg

	Table 2 - Project Cost Information Based on Years 1-5       (See General Notes C & D Above)												
Stormwater Retrofit Practice	Weighted Average (Design + Construction) per KG	Weighted Average Plus 15% Contingency & 5 Year Inflation (3% per year) per KG	Lowest Design + Construction (Plus Contingency & Inflation) per KG	Highest Design + Construction (Plus Contingency & Inflation) per KG									
Subsurface Infiltration	\$119,244	\$158,972	\$62,502	\$360,904									
Water Quality Pond	\$91,904	\$122,523	\$42,012	\$288,177									
Surface Filters	\$50,372	\$67,154	\$40,495	\$145,043									
Dry Swale	\$67,925	\$90,555	\$37,330	\$147,033									
Stormfilter	\$54,236	\$72,305	\$51,653	\$245,240									
Channel Stabilization	\$32,725	\$43,627	\$10,091	\$68,685									
Bioretention	\$165,648	\$220,836	\$204,506	\$244,995									

#### Footnotes:

1 Previously Year 3 Project (formerly Pat-MB-05), fully designed and requires construction easement.

2 Project proposes stabilization of eroded stream in Connecticut. Contributing drainage area and proposed stabilization is within EOH Watershed and stream is tributary to Putnam Lake in Patterson.

3 Project proposes retrofitting existing stormwater detention practice to water quality pond.

4 Estimated project costs for channel stabilization projects within classified streams have been increased by a factor of 50% to account for natural and more expensive stabilization measures (in conjunction with stone riprap) that may potentially be required by the NYSDEC. Historical cost range information has also been omitted for these projects since historical cost data only exists for channels stabilized exclusively with riprap.



# APPENDIX B: STORMWATER RETROFIT CONCEPT PLANS AND CALCULATIONS







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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:VB-1Prepared for:EOHCPrepared by:REDProject County:Putnam

#### "VB-1: PUTNAM TERRACE"

A =	2.76297	acres	where:	A =	Contributing Area (acres)
=	0.658	23.81%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calc	ulated)=	0.2643		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.2643			
WQv (ad	cre-ft) =	0.073			
WQv (cu	ı-ft) =	3181			
**Minim	m Ry = 0	2 when determin			ated Ry when determining phoephorus loadin

#### \*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.2643		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	2.76297		Rv =	Runoff Coefficient	
C =	0.43		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0.76
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.24
Develped Open Space	0
Weighted "C":	0.43



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	<b>59%</b>
P Load>	<b>2.90</b> lb/yr
	<b>1.31</b> kg/yr
P Removal>	<b>1.71</b> lb/yr
	<b>0.78</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	2.8	Phosphorus Loading (kg/yr) 1.3		
Water Quality Volume (cf)	3181	Phosphorus Reduction (kg/yr)	0.78	

#### ASSUMPTIONS/COMMENTS:

Install practice in within "paper street" owned by the Village of Brewster.

Drainage area consists of a residential district.

A diversion swale will be required for this location.

Further exploration should be completed to determine if additional areas could be directed to this location.

Map Output

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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:VB-2Prepared for:EOHCPrepared by:REDProject County:Putnam

#### "VB-2: RAILROAD AVE"

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	v)(A)] /12
A = I =	3.44 1.86	acres 54.07%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.5366		WQv =	Water Quality Volume
Rv (min)	** =	0.5366			
WQv (acre-ft) = 0.185					
WQv (cu	I-ft) =	8041			
**Minimum Rv = 0.2 when determining WQv.			nining WQv. l	Jse calcula	ted Rv when determining phosphorus loading.

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	C x A x 0.1	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.5366		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3.44		Rv =	Runoff Coefficient
C =	0.46		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0.46
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.54
Develped Open Space	0
Weighted "C":	0.46



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>7.78</b> lb/yr
	<b>3.53</b> kg/yr
P Removal>	<b>4.59</b> lb/yr
	<b>2.08</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	3.4	Phosphorus Loading (kg/yr) 3.		
Water Quality Volume (cf)	8041	Phosphorus Reduction (kg/yr)	2.08	

#### ASSUMPTIONS/COMMENTS:

Install practices within existing parking lot property that is owned by NYCDEP and leased to the Village of Brewster for commuter use.

Add curbs along Park Street to contain practice at the parking lot end cap.

The parking lot entrance is onto Park Street.

Bioretention could be considered as an alternative practice because it has a larger phosphorus removal capacity. Further investigation may find additional area that drains to this catchment area.

Map Output

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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:VB-3Prepared for:EOHCPrepared by:REDProject County:Putnam

#### "VB-3: SOUTHEAST MUSEUM/BREWSTER LIBRARY"

WATER QUALITY VOLUME: WQv(acr			WQv(acre-fee	feet) = [(P)(Rv)(A)]/12				
A =   = P =	1.71 1 1.2	acres 58.48% inches	where:	A =   = P =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in)			
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]			
Rv (calcu	lated)=	0.5763		WQv =	Water Quality Volume			
<b>Rv</b> (min)	** =	0.5763						
WQv (ac	re-ft) =	0.099						
WQv (cu	-ft) =	4293						
**Minimum $Rv = 0.2$ when determining WQv.			mining WQv. I	Use calcula	ated Rv when determining phosphorus loading.			

#### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103				
P =	45	where:	P Load=	Annual load (kg/yr)		
Pj =	0.9		P =	Annual Rainfall (inches)		
Rv =	0.5763		Pj =	Fraction of rainfall producing Runoff = 0.9		
A =	1.71		Rv =	Runoff Coefficient		
C =	0.43		C =	Pollutant Concentration (mg/l)		
			A =	A = Contributing Area (acres)		

Land Use	% of Total Area
Residential	0
Commercial	0.42
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.58
Develped Open Space	0
Weighted "C":	0.43



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	3.92 lb/yr
	<b>1.78</b> kg/yr
P Removal>	2.31 lb/yr
	<b>1.05</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	1.7 Phosphorus Loading (kg/yr) 1.78			
Water Quality Volume (cf)	4293	Phosphorus Reduction (kg/yr)	1.05	

#### **ASSUMPTIONS/COMMENTS:**

Install practice within existing parking lot property that is owned by the Town of Southeast.

Alternatively this practice could be installed across Marvin Ave. on Village of Brewster Property.

Bioretention could be considered as an alternative practice because it has a larger phosphorus removal capacity. Bioretention could be considered as an alternative practice at this location.

Map Output

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### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Carmel-1A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

#### Carmel-1A: Arborview - A

WATER QUALITY VOLUME: WQv(acre-feet) = [(P)(Rv)(A)] /12

A =	31.6	acres	where:	A =	Contributing Area (acres)
1 =	9	28.48%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated	)=	0.3063		WQv =	Water Quality Volume
Rv (min)** =		0.3063			
WQv (acre-ft)	) =	0.968			
WQv (cu-ft) =		42166			
**Minimum Rv	/= 0.2	2 when determi	ining WQv. I	Use calcul	ated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3063		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	31.6		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	36.49 lb/yr
	16.55 kg/yr
P Removal>	20.07 lb/yr
	9.10 kg/yr

7.28 kg/yr Assume 80% of WQv treated

#### Summary:

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	31.6 Phosphorus Loading (kg/yr) 16.55			
Water Quality Volume (cf)	42166	Phosphorus Reduction (kg/yr)	7.28	



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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Carmel-1B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

#### Carmel-1B: Arborview - B

WATER QUALITY VOLUME: WQv(acre-feet) = [(P)(Rv)(A)] /12

A =	17.9	acres	where:	A =	Contributing Area (acres)
1 =	5.27	29.44%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculate	d)=	0.3150		WQv =	Water Quality Volume
Rv (min)** =		0.3150			
WQv (acre-fi	t) =	0.564			
WQv (cu-ft)	=	24559			
**Minimum R	v = 0.	2 when determi	ining WQv. I	Use calcul	ated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3150		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	17.9		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41


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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	21.25 lb/yr
	9.64 kg/yr
P Removal>	11.69 lb/yr
	5.30 kg/yr

4.24 kg/yr	Assume 80% of WQv treated
------------	---------------------------

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	17.9	Phosphorus Loading (kg/yr)	9.64
Water Quality Volume (cf)	24559	Phosphorus Reduction (kg/yr)	5.30



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	RENNIA ENGINEERING DESIGN, MLK COLLONNOMENTAL - TENCTIAN. IN ADDRESS TAX AND TO ADDRESS	Woodard & Curren Engineering PA PC 708 Westcheeber Avenue, Suite L2 While Plains, New York 19664 850,007,4580   www.weoderdcarran.com	WOODARD COMMITMENT & INTEGRITY DRIVE REBULTS
Carmel Multi Pana Carmel	A A A A A A A A A A A A A A A A A A A	STORMWATER RETROFIT CONCEPT PLAN	SOMED BY: CRP /ROL CHECKED BY: LUP XWN BY: CRP /ROL ELEANORORIVE_CONCEPTPLAN_FIDUR
AP: SCALE: 1* = 4000' Vorki Street Mep			DES
ATION SHOWN HEREON TAKEN FROM COUNTY & HYDROGRAPHIC INFORMATION SHOWN HERE EW YORK CITY DEPARTMENT OF ENVIRONMEN UREAU OF WATER SUPPLY, 2012, SUBJECT TO EMENT BETWEEN NYCDEP & EOHWC. TE WETLAND INFO TAKEN FROM CORNELL UNIN FORMATION REPOSITORY. ITILITY INFORMATION SHOWN HEREON PROVIE OR CONCEPTUAL DESIGN PURPOSES ONLY. US VALUES INCLUDED IN THIS RETROFIT PLAN UES. FINAL SIGNED AND SEALED PHOSPHORU JLATIONS WILL NEED TO BE PERFORMED IN MITH THE EOHWC DESIGN MANUAL CONSISTEN PROVED NYSDEC "ALTERNATIVE CHANNEL FORMULA". THE FINAL CALCULATIONS SHOULD DNFIRM CHANNEL DIMENSIONS, AND A COMPLE COMPUTATIONS OF ALL INPUT PARAMETERS U	Y TAX CON TAL GIS DATA VERSITY VED BY I ARE IS IT WITH D INCLUDE TE SED IN	CHANNEL STABILIZATION	TOWN OF CARMEL
IVE CHANNEL STABILIZATION FORMULA*, INCLU VIDEXES.	JDING THE	DATE: 8/1 SCALE: 1	'-60'
	]	CARM	EL-2

Channel ID	A	В	C	D	E	F
Channel Depth - y (ft)	2.0	5.0				
Channel Bottom Width - B (ft)	6.0	10.0				
Channel Top Width -T (ft)	8.0	12.0				
Vetted Perimeter Calculation- P (ft)	10.47	20.20	5			
Channel Length-L (ft)	210	140				
Soil Erosion Depth-D (ft)	0.065	0.065				
Soil Erosion Volume-V (ft <sup>3</sup> )	142.9	183.8				
Weight* (lbs)	13,579.7	17,461.2				
Weight (Kg)	6,159.8	7,920.4				
P Load** (mg/Yr)	1,847,931.3	2,376,120.7				j.
P Load (Kg/Yr)	1.85	2.38				

ESTIMATED TOTAL (KG/YR): 4.22

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soll (typ. 300 mg/kg)







WATER OUALITY VOLUME:

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Carmel-4A
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Carmel-4A: Putnam Hospital Center - A

THAT EN S	OALITI	TOLOML.	WGW across	er = th M	14/(4)//12
A =	3.8	acres	where:	A =	Contributing Area (acres)
1 =	3.8	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcul	ated)=	0.9500		WQv =	Water Quality Volume
Rv (min)*	*=	0.9500			
WQv (acr	e-ft) =	0.361			
WQv (cu-	ft) =	15725			
**Minimun	n Rv = 0.	2 when deter	mining WQv.	Use calcul	ated Rv when determining phosphorus loading.

WOu/acro-foot) - I/PI/Pu//A)1/12

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3.8		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	16.59 lb/yr
	7.53 kg/yr
P Removal>	9.13 lb/yr
	4.14 kg/yr

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	3.8	Phosphorus Loading (kg/yr)	7.53
Water Quality Volume (cf)	15725	Phosphorus Reduction (kg/yr)	4.14



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Carmel-4B
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Carmel-4B: Putnam Hospital Center - B

WATER C	UALITY	VOLUME:	WQv(acre-fe	et) = [(P)(F	lv)(A)]/12
A =	5.7	acres	where:	A =	Contributing Area (acres)
P =	1.2	inches		P=	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcul	ated)=	0.9500		WQv =	Water Quality Volume
Rv (min)**	'=	0.9500			
WQv (acr	e-ft) =	0.542			
WQv (cu-	ft) =	23588			
**Minimun	h Rv = 0.	2 when deter	mining WQv.	Use calcula	ated Rv when determining phosphorus loading.

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	5.7		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	24.89 lb/yr
	11.29 kg/yr
P Removal>	13.69 lb/yr
	6.21 kg/yr

Proposed Retrofit Practice Wet ED Pond			
Drainage Area (acres)	5.7	Phosphorus Loading (kg/yr)	11.29
Water Quality Volume (cf)	23588	Phosphorus Reduction (kg/yr)	6.21









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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Carmel-5A
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Carmel-5A: Putnam Plaza - A

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	iv)(A)]/12
A =	1.17	acres	where:	A =	Contributing Area (acres)
1 =	1.17	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	(ated)=	0.9500		WQv =	Water Quality Volume
Rv (min)*	*=	0.9500			
WQv (ac	re-ft) =	0.111			
WQv (cu	-ft) =	4842			

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### WQv PEAK FLOW:

Based upon NYSDE	Stormwater	Manual,	Appendix B-2
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Tc =	0.08 hours	Tc =	Time of Concentration (hours)
CN =	99	CN =	Curve Number
qu =	569.691	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.18727 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	$P Load = P \times P j \times R v \times X$	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.17		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	5.11 lb/yr
	2.32 kg/yr
P Removal>	2.04 lb/yr
	0.93 kg/yr

Proposed Retrofit Practice	Stormfilter			
Drainage Area (acres)	1.2	Phosphorus Loading (kg/yr)	2.32	
Water Quality Volume (cf)	4842	Phosphorus Reduction (kg/yr)	0.93	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Carmel-5B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Carmel-5B: Putnam Plaza - B

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(F)	Rv)(A)]/12
A =	0.52	acres	where:	A =	Contributing Area (acres)
P =	1.2	inches		P=	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calci	ulated)=	0.9500		WQv =	Water Quality Volume
Rv (min)	** =	0.9500			
WQv (ad	cre-ft) =	0.049			
WQv (cu	1-ft) =	2152			

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.08 hours	Tc =	Time of Concentration (hours)
CN =	99	CN =	Curve Number
qu =	569.691	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	0.52768 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	$P Load = P \times P j \times R v \times X$	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	0.52		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	2.27 lb/yr
	1.03 kg/yr
P Removal>	0.91 lb/yr
	0.41 kg/yr

Proposed Retrofit Practice	Stormfilter			
Drainage Area (acres)	0.5	Phosphorus Loading (kg/yr)	1.03	
Water Quality Volume (cf)	2152	Phosphorus Reduction (kg/yr)	0.41	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Carmel-5C Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Carmel-5C: Putnam Plaza - C

WATER OUALITY VOLUME.

WATER	JUALITT	VOLUME.	waviacie-ie	ei) = I(r)(r)	14/(4/)/12
A =	1.66	acres	where:	A =	Contributing Area (acres)
1 =	1.66	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	(ated)=	0.9500		WQv =	Water Quality Volume
Rv (min)*	*=	0.9500			
WQv (aci	re-ft) =	0.158			
WQv (cu	-ft) =	6869			
ant dimineret	- D. 0	O under an electronic	mining WOW	line entruit	stad Duudee determining cheechange landi

M/Ou/ages fact) - I/DI/Du//A)1/42

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### WQv PEAK FLOW:

Based upon NYSDE	Stormwater	Manual,	Appendix B-2
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Tc =	0.08 hours	Tc =	Time of Concentration (hours)
CN =	99	CN =	Curve Number
qu =	569.691	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.6845 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	$P Load = P \times P j \times R v \times X$	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.66		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	7.25 lb/yr
	3.29 kg/yr
P Removal>	2.90 lb/yr
	1.32 kg/yr

Proposed Retrofit Practice Stormfilter			
Drainage Area (acres)	1.7	Phosphorus Loading (kg/yr)	3.29
Water Quality Volume (cf)	6869	Phosphorus Reduction (kg/yr)	1.32



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Carmel-5D Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Carmel-5D: Putnam Plaza - D

WATER OUALITY VOLUME.

MAILA	GOALITT	VOLUME.	wowlacie.iei	et = ttr M	iv/(A)//12
A =	1.28	acres	where:	A =	Contributing Area (acres)
1 =	1.28	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.9500		WQv =	Water Quality Volume
Rv (min)	** =	0.9500			
WQv (ac	re-ft) =	0.122			
WQv (cu	1-ft) =	5297			
**Minimu	Im Rv = 0.	2 when deter	mining WQv.	Use calcul	ated Rv when determining phosphorus loading.

W/Ou/acro-foot) - I/PI/Pu//A)1/12

#### WQv PEAK FLOW:

Based upon	NYSDEC	Stormwater	Manual.	Appendix B-2
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Tc =	0.08 hours	Tc =	Time of Concentration (hours)
CN =	99	CN =	Curve Number
qu =	569.691	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.29889 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	$P Load = P \times P j \times R v \times X$	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.28		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	0.50



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	5.59 lb/yr
	2.54 kg/yr
P Removal>	2.24 lb/yr
	1.01 kg/yr

Proposed Retrofit Practice			
Drainage Area (acres)	1.3	Phosphorus Loading (kg/yr)	2.54
Water Quality Volume (cf)	5297	Phosphorus Reduction (kg/yr)	1.01







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Carmel-7
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Carmel-7: Tanya Lane

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	iv)(A)]/12
A =   =	22.47 6.74	acres 30.00%	where:	A = 1 =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calc	ulated)=	0.3200		WQv =	Water Quality Volume
Rv (min)	**=	0.3200			
WQv (a	cre-ft) =	0.719			
WQv (c	u-ft) =	31317			
**Minimu	um Etv - 0	2 when date	mining WOw 1	lee colcul	ated By when determining phoephorus loadin

Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### WQv PEAK FLOW:

Based upon NYSDE	Stormwater	Manual,	Appendix B-2
------------------	------------	---------	--------------

Tc =	0.45 hours	Tc =	Time of Concentration (hours)
CN =	88	CN =	Curve Number
qu =	406.531	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	5.48016 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	$P Load = P \times P j \times R v \times X$	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3200		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	22.47		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond	
Removal Efficiency:	55%	
P Load>	27.10 lb/yr	
	12.29 kg/yr	
P Removal>	14.90 lb/yr	
	6.76 kg/yr	

5.41 kg/yr Assume 80% of WQV treated	5.41 kg/yr	Assume 80% of WQv treated
--------------------------------------	------------	---------------------------

Proposed Retrofit Practice	Wet ED Pond				
Drainage Area (acres)	22.5	Phosphorus Loading (kg/yr)	12.29		
Water Quality Volume (cf)	31317	Phosphorus Reduction (kg/yr)	5.41		



Channel ID	A	в	c	D	E	F
Channel Depth - y (#)	6.0					
Channel Bottom Width - B (ft)	15.0					
Channel Top Width -T (ft)	20.0					
Wetted Perimeter Calculation- P (ft)	28.00					
Channel Length-L (ft)	340					
Soil Erosion Depth-D (ft)	0.065					
Soil Erosion Volume-V (ft <sup>3</sup> )	618.8					
Weight* (lbs)	58,786.0					
Weight (Kg)	26,665.3					
P Load** (mg/Yr)	7,999,598.9					
P Load (Kg/Yr)	8.00					

ESTIMATED TOTAL (KG/YR): 8.00

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [{8/3}\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

Channel ID	A	в	c	D	E	F
Channel Depth - y (#)	6.0					
Channel Bottom Width - B (ft)	10.0					
Channel Top Width -T (ft)	15.0					
Wetted Perimeter Calculation- P (ft)	23.00					
Channel Length-L (ft)	300					
Soil Erosion Depth-D (ft)	0.065					
Soil Erosion Volume-V (ft <sup>3</sup> )	448.5					
Weight* (lbs)	42,607.5					
Weight (Kg)	19,326.8					
P Load** (mg/Yr)	5,798,028.6					
P Load (Kg/Yr)	5.80					

ESTIMATED TOTAL (KG/YR): 5.80

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [{8/3}\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-1
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Kent-1: Kent Highway Garage

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R)]	Iv)(A)]/12
A =     =   P =	2.3 2.3 1.2	acres 100.00% inches	where:	A =   = P =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in)
Rv (calcu WQv (aci WQv (cu	lated)= re-ft) = -ft) =	0.9500 0.219 9518		Rv = WQv =	Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQv PEAK Based up	FLOW: on NYSD	EC Stormwa	ter Manual. App	endix B-2	
Tc =	0.15	hours		Tc =	Time of Concentration (hours)

1C =	0.15 nours	IC =	Time of Concentration (nours)
CN =	99	CN =	Curve Number
qu =	531.274	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	2.17656 CFS	Qp =	Peak Discharge (CFS)

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x P j x R v x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.3		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted *C	: 0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	10.04 lb/yr
	4.56 kg/yr
P Removal>	4.02 lb/yr
	1.82 kg/yr

Proposed Retrofit Practice	Stormfilter			
Drainage Area (acres)	2.3	Phosphorus Loading (kg/yr)	4.56	
Water Quality Volume (cf)	9518	Phosphorus Reduction (kg/yr)	1.82	







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent - 2 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-2: Montrose Drive Outfall

A =	61.5	acres	where:	A =	Contributing Area (acres)
1 =	18.5	30.08%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.3207		WQv =	Water Quality Volume
WQv (ac	re-ft) =	1.973			
WQv (cu	-ft) =	85922			

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3207		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	61.5		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted *C":	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Multiple Pond
Removal Efficiency:	76%
P Load>	74.35 lb/yr
	33.73 kg/yr
P Removal>	56.51 lb/yr
	25.63 kg/yr

20.50 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Multiple Pond			
Drainage Area (acres)	61.5	Phosphorus Loading (kg/yr) 33		
Water Quality Volume (cf)	85922	Phosphorus Reduction (kg/yr)	20.50	



#### LOCATION MAP: SCALE: 1" = 3000"

Source: ArcGIS World Street Map

#### **GENERAL NOTES:**

**Materia** in

Laurel

- PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING.
- TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER SUPPLY, 2012, SUBJECT TO GIS DATA SHARING AGREEMENT BETWEEN NYCDEP & EOHWC.
- NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL INFORMATION REPOSITORY.
- ANY EXISTING UTILITY INFORMATION SHOWN HEREON PROVIDED BY MUNICIPALITY FOR CONCEPTUAL DESIGN PURPOSES ONLY.

#### SITE SPECIFIC NOTES:

- DRAINAGE AREA INDICATED IS INTENDED AS AN ESTIMATE FOR CONCEPTUAL USE ONLY, FURTHER EVALUATION OF ACTUAL SUBCATCHMENT BOUNDARIES MUST BE COMPLETED AS PART OF DETAILED DESIGN.
- PROPOSED SRP IS LOCATED ON PRIVATE PROPERTY, COORDINATION WITH THE PROPERTY OWNER WILL BE REQUIRED TO OBTAIN EASEMENTS FOR ANY WORK PERFORMED.





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-3 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-3: Chuang Yen Monastery

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
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A =	3	acres	where:	A =	Contributing Area (acres)
1 =	3	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.9500		WQv =	Water Quality Volume
WQv (acre-f	t) =	0.285			
WQv (cu-ft)	=	12415			

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pi =	Fraction of rainfall producing Runoff = 0.9
A =	3		Rv =	Runoff Coefficient
C =	0.43		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0.73
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.27
Develped Open Space	0
Weighted "C":	0.43


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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter		
Removal Efficiency:	59%		
P Load>	11.38 lb/yr		
	5.16 kg/yr		
P Removal>	6.71 lb/yr		
	3.05 kg/yr		

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	3.0 Phosphorus Loading (kg/yr) 5.16		
Water Quality Volume (cf)	12415	Phosphorus Reduction (kg/yr)	3.05





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-4
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

#### Kent-4: Lakeview Restaurant

WATER	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Iv)(A)]/12
A =	2.24	acres	where:	A =	Contributing Area (acres)
=	0.7	31.25%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.3313		WQv =	Water Quality Volume

WQv (acre-ft) =	0.074
WQv (cu-ft) =	3232

WQv	PEAK	FLOW:
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Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.15 hours	Tc =	Time of Concentration (hours)
CN =	89	CN =	Curve Number
qu =	618.115	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	0.85995 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAxO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3313		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.24		Rv =	Runoff Coefficient
C =	0.44		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0.69
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.31
Develped Open Space	0
Weighted "C":	0.44



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	2.99 lb/yr
	1.35 kg/yr
P Removal>	1.19 lb/yr
	0.54 kg/yr

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	2.2	Phosphorus Loading (kg/yr)	1.35
Water Quality Volume (cf)	3232	Phosphorus Reduction (kg/yr)	0.54





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-5 A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-5 A: Lake Carmel

WATER QUALITY VOLUME:		WQv(acre-feet) = [(P)(Rv)(A)]/12			
A =	42	acres	where:	A =	Contributing Area (acres)
1000	107	20.249/		1 -	Impopulate Aros (acroc/9/

=	12.1	30.24%	=	Impervious Area (acres/%)
P =	1.3	2 inches	P =	90th Percentile Rainfall Event Number (in)
			Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculate	ed)=	0.3221	WQv =	Water Quality Volume
Rv (min)** =		0.3221		
WQv (acre-	ft) =	1.353		
WQv (cu-ft)	=	58937		
and distances I	Der 1	O when determini	an WOr Line anion	lated Duuden determining sharehous landis

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3221		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	42		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	51.00 lb/yr
	23.13 kg/yr
P Removal>	28.05 lb/yr
	12.72 kg/yr

10.18 kg/yr	Assume 80% o	f WQv treated
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Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	42.0	Phosphorus Loading (kg/yr)	23.13	
Water Quality Volume (cf)	58937	Phosphorus Reduction (kg/yr)	10.18	







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 B
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

### Kent-5 B: Lake Carmel

Number (in)
09(I)]
1

#### WQv PEAK FLOW:

Based up	on NYSDEC Stormwater Ma	inual. Appendix B-2	
Tc =	0.15 hours	Tc =	Time of Concentration (hours)
CN-	80	CN-	Curve Number

CN =	89	CN =	Curve Number
qu =	618.115	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.4545 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x P j x R v x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3586		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3.5		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 Actively Grazed Pasture 0 Forest 0 Impervious 0 0 Develped Open Space Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	4.73 lb/yr
	2.15 kg/yr
P Removal>	1.89 lb/yr
	0.86 kg/yr

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	3.5	Phosphorus Loading (kg/yr)	2.15
Water Quality Volume (cf)	5467	Phosphorus Reduction (kg/yr)	0.86



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 C
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

## Kent-5 C: Lake Carmel

WATER C	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(F)	Tv)(A)]/12
A =	13.8	acres	where:	A =	Contributing Area (acres)
1=	4.2	30.43%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcul	ated)=	0.3239		WQv =	Water Quality Volume
WQv (acr	e-ft) =	0.447			
WQv (cu-	ft) =	19471			

#### WQv PEAK FLOW:

Based	upon NYSDEC S	ormwater Manual. Appendix B-	2
Tc =	0.25 hour	Tc =	Time of Concentration (hours)
CN =	88	CN =	Curve Number
qu =	513.485	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	4.30364 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3239		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	13.8		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 Actively Grazed Pasture 0 Forest 0 Impervious 0 0 Develped Open Space Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	16.85 lb/yr
	7.64 kg/yr
P Removal>	6.74 lb/yr
	3.06 kg/yr

2.45 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	13.8	Phosphorus Loading (kg/yr)	7.64
Water Quality Volume (cf)	19471	Phosphorus Reduction (kg/yr)	2.45



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-5 D Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-5 D: Lake Carmel

WATER O	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	4.9	acres	where:	A =	Contributing Area (acres)
1 =	1.5	30.61%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcul	ated)=	0.3255		WQv =	Water Quality Volume
WQv (acr	e-ft) =	0.160			
WQv (cu-	ft) =	6948			

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.16 hours	Tc =	Time of Concentration (hours)
CN =	88	CN =	Curve Number
qu =	595.594	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.7812 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3255		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	4.9		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted *C*:	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	6.01 lb/yr
	2.73 kg/yr
P Removal>	2.40 lb/yr
	1.09 kg/yr

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	4.9	Phosphorus Loading (kg/yr)	2.73
Water Quality Volume (cf)	6948	Phosphorus Reduction (kg/yr)	1.09





#### LOCATION MAP: SCALE: 1" = 3000"

Source: ArcGIS World Street Map

#### **GENERAL NOTES:**

- PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING, TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER SUPPLY, 2012, SUBJECT TO GIS DATA SHARING AGREEMENT BETWEEN NYCDEP & 1. 2.
- EOHWC. NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL INFORMATION REPOSITORY. ANY EXISTING UTILITY INFORMATION SHOWN HEREON PROVIDED BY MUNICIPALITY 3,
- 4. FOR CONCEPTUAL DESIGN PURPOSES ONLY,
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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-5 E Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-5 E: Lake Carmel

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	14	acres	where:	A =	Contributing Area (acres)
1 =	4.3	30.71%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.3264		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.457			
WQv (cu	-ft) =	19907			

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.3 hours	Tc =	Time of Concentration (hours)
CN =	88	CN =	Curve Number
qu =	479.823	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	4.11149 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3264		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	14		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	17.23 lb/yr
	7.81 kg/yr
P Removal>	6.89 lb/yr
	3.13 kg/yr

2.50 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	14.0	Phosphorus Loading (kg/yr)	7.81
Water Quality Volume (cf)	19907	Phosphorus Reduction (kg/yr)	2.50





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 F
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

### Kent-5 F: Lake Carmel

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	7	acres	where:	A =	Contributing Area (acres)
1 =	2.2	31.43%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calci	ulated)=	0.3329		WQv =	Water Quality Volume
WQv (ad	cre-ft) =	0.233			- 1971 - 1946 D. 4 - 1974 - 1977 - 1977 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 - 1971 -
WQV (CL	1-ft) =	10149			

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.2 hours	Tc =	Time of Concentration (hours)
CN =	89	CN =	Curve Number
qu =	565.468	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	2.47039 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3329		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	7		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	8.78 lb/yr
	3.98 kg/yr
P Removal>	4.83 lb/yr
	2.19 kg/yr

1.75 kg/yr	Assume 80% of WQv treated
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Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	7.0 Phosphorus Loading (kg/yr) 3.9		
Water Quality Volume (cf)	10149	Phosphorus Reduction (kg/yr)	1.75



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 G
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Kent-5 G: Lake Carmel

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WATER	QUALITY	VOLUME:	WQv(acre-fee	P(P) = l(P)(P)	iv)(A)]/12
A =	8.3	acres	where:	A =	Contributing Area (acres)
1 =	2.5	30.12%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.3211		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.267			
WQv (cu	-ft) =	11609			

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2 Tc = 0.2 hours Tc = Time of Concentration (hours) CN = 88 CN = Curve Number

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			Contro Homoor
qu =	554.75	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	2.77202 CFS	Qp =	Peak Discharge (CFS)
ab -	ETTENE OF O	sap -	i can biograd go (or o)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x P j x R v x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3211		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	8.3		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 Actively Grazed Pasture 0 Forest 0 Impervious 0 Develped Open Space 0 Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	10.05 lb/yr
	4.56 kg/yr
P Removal>	5.52 lb/yr
	2.51 kg/yr

2.00 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	8.3 Phosphorus Loading (kg/yr) 4.5		
Water Quality Volume (cf)	11609	Phosphorus Reduction (kg/yr)	2.00





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-5 H Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

### Kent-5 H: Lake Carmel

WATER C	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	9.3	acres	where:	A =	Contributing Area (acres)
1 =	2.9	31.18%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcul	ated)=	0.3306		WQv =	Water Quality Volume
WQv (acr	e-ft) =	0.308			
WQv (cu-	ft) =	13395			

#### WQv PEAK FLOW:

Based u	upon NYSD	EC Stormwater Ma	anual. Appendix B-2	
Tc =	1	hours	Tc =	Time of Concentration (hours)
CN =	89		CN =	Curve Number
qu =	#NUMI		qu =	Unit Peak Discharge (cfs/mi²/inch)
Qp =	#NUM!	CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3306		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	9.3		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted *C*:	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	11.59 lb/yr
	5.26 kg/yr
P Removal>	6.37 lb/yr
	2.89 kg/yr

	2.31 kg/yr	Assume 80% of WQv treated
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Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	9.3	Phosphorus Loading (kg/yr)	5.26
Water Quality Volume (cf)	13395	Phosphorus Reduction (kg/yr)	2.31



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 I
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Kent-5 I: Lake Carmel

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%)
Event Number (in)
+ 0.009(I)]
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#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.2 hours	Tc =	Time of Concentration (hours)
CN =	89	CN =	Curve Number
qu =	565.468	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	3.14895 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3300		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	9		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted *C*:	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	11.19 lb/yr
	5.08 kg/yr
P Removal>	6.16 lb/yr
	2.79 kg/yr

2.23 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	9.0	Phosphorus Loading (kg/yr)	5.08
Water Quality Volume (cf)	12937	Phosphorus Reduction (kg/yr)	2.23





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

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Project #:	Kent-5 J
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Kent-5 J: Lake Carmel

WATER	QUALITY	VOLUME:	WQv(acre-fee	P(P) = l(P)(P)	iv)(A)]/12
A =	28	acres	where:	A =	Contributing Area (acres)
1 =	8.5	30.36%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.3232		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.905			
WQv (cu	-ft) =	39422			

#### WQv PEAK FLOW:

Based	upon NYSDE	C Stormwater Mar	nual. Appendix B-2	
Tc =	0.34 h	ours	Tc =	Time of Concentration (hours)
CN =	88		CN =	Curve Number
qu =	456.895		qu =	Unit Peak Discharge (cfs/mi²/inch)
Qp =	7.75294 C	FS	Qp =	Peak Discharge (CFS)
Qp =	7.75294 0	FS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3232		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	28		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 0 Actively Grazed Pasture Forest 0 Impervious 0 0 Develped Open Space Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond	
Removal Efficiency:	55%	
P Load>	34.11 lb/yr	
	15.47 kg/yr	
P Removal>	18.76 lb/yr	
	8.51 kg/yr	

4.26 kg/yr Assume 50% of WQv treated

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	28.0	Phosphorus Loading (kg/yr)	15.47	
Water Quality Volume (cf)	39422	Phosphorus Reduction (kg/yr)	4.26	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 K
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

### Kent-5 K: Lake Carmel

WATER	QUALITY	VOLUME:	WQv(acre-fee	P(P) = [(P)(P)	Tv)(A)]/12
A =	28.5	acres	where:	A =	Contributing Area (acres)
1 =	8.8	30.88%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calci	ulated)=	0.3279		WQv =	Water Quality Volume
WQv (ad	cre-ft) =	0.935			
WQV (CL	1-ft) =	40707			

#### WQv PEAK FLOW:

Based u	upon NYSDEC Stormwater M	lanual. Appendix B-2	
Tc =	0.34 hours	Tc =	Time of Concentration (hours)
CN =	88	CN =	Curve Number
qu =	456.895	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	8.00566 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3279		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	28.5		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 Actively Grazed Pasture 0 Forest 0 Impervious 0 0 Develped Open Space Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	35.22 lb/yr
	15.98 kg/yr
P Removal>	19.37 lb/yr
	8.79 kg/yr
	8.79 kg/yr

4.39 kg/yr Assume 50% of WQv treated

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	28.5	Phosphorus Loading (kg/yr)	15.98	
Water Quality Volume (cf)	40707	Phosphorus Reduction (kg/yr)	4.39	






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(hours)

## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Kent-5 L
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

## Kent-5 L: Lake Carmel

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WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = l(P)(P)	iv)(A)]/12
A =	9.1	acres	where:	A =	Contributing Area (acres)
1 =	2.8	30.77%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	(lated)=	0.3269		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.298			
WQv (cu	-ft) =	12959			

#### WQv PEAK FLOW:

Based u	pon NYSDEC Stormwater M	lanual. Appendix B-2	
Tc =	0.2 hours	Tc =	Time of Concentration
CN =	88	CN =	Curve Number
124124	FF 4 75	122.2 C	Linit Deals Discharge /

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qu =	554.75	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	3.09447 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3269		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	9.1		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

#### Weighted Loading Coefficients Land Use % of Total Area Residential 1 Commercial 0 Industrial 0 0 Actively Grazed Pasture Forest 0 Impervious 0 0 Develped Open Space Weighted "C": 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	11.21 lb/yr
	5.09 kg/yr
P Removal>	4.49 lb/yr
	2.03 kg/yr

1.63 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	9.1	Phosphorus Loading (kg/yr)	5.09
Water Quality Volume (cf)	12959	Phosphorus Reduction (kg/yr)	1.63



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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-5 M Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Kent-5 M: Lake Carmel

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	13.6	acres	where:	A =	Contributing Area (acres)
1 =	4.2	30.88%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calc	ulated)=	0.3279		WQv =	Water Quality Volume
WQv (ad	re-ft) =	0.446			
WQv (cu	1-ft) =	19428			

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.25	hours	Tc =	Time of Concentration (hours)
CN =	88		CN =	Curve Number
qu =	513.485		qu =	Unit Peak Discharge (cfs/mi²/inch)
Qp =	4.29401	CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x P j x R v x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3279		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	13.6		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	16.81 lb/yr
	7.63 kg/yr
P Removal>	6.72 lb/yr
	3.05 kg/yr

2.44 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter		
Drainage Area (acres)	13.6	Phosphorus Loading (kg/yr)	7.63
Water Quality Volume (cf)	19428	Phosphorus Reduction (kg/yr)	2.44



Kent Elementary School - B

Sity Of New York

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#### LOCATION MAP: SCALE: 1" = 6000"

## Source: ArcGIS World Street Map

#### **GENERAL NOTES:**

- PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING,
  TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER SUPPLY, 2012, SUBJECT TO GIS DATA SHARING AGREEMENT BETWEEN NYCDEP & EOHWC.
- NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL INFORMATION REPOSITORY.
- ANY EXISTING UTILITY INFORMATION SHOWN HEREON PROVIDED BY MUNICIPALITY FOR CONCEPTUAL DESIGN PURPOSES ONLY.

#### SITE SPECIFIC NOTES:

- DRAINAGE AREA INDICATED IS INTENDED AS AN ESTIMATE FOR CONCEPTUAL USE ONLY. FURTHER EVALUATION OF ACTUAL SUBCATCHMENT BOUNDARIES MUST BE COMPLETED AS PART OF DETAILED DESIGN.
- PROPOSED SRP IS LOCATED ON CARMEL SCHOOL DISTRICT PROPERTY. COORDINATION WITH THE SCHOOL DISTRICT WILL BE REQUIRED TO FURTHER INVESTIGATE SITE, OBTAIN AS-BUILT SURVEY INFORMATION OF EXISTING DETENTION EXISTING COLLECTION SYSTEM AND TO OBTAIN EASEMENTS FOR ANY WORK PERFORMED.

PROPOSED STORMWATER RETROFIT PROJECT: SURFACE SAND FITLER

FARMERS MILLS ROAD

EST. PHOSPHORUS REMOVAL: 2.86 KG/YR SEE ATTACHED CALCULATION SHEET







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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-6 A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

## Kent-6 A: Kent Elementary School - A

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)] /12
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A =	3 acr	es	where:	A =	Contributing Area (acres)
1 =	3 1	00.00%		1 =	Impervious Area (acres/%)
P =	1.2 incl	hes		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)=		0.9500		WQv =	Water Quality Volume
Rv (min)** =		0.9500			
WQv (acre-ft) =	-	0.285			
WQv (cu-ft) =		12415			
**Minimum Rv -	= 0.2 wi	hen determi	ning WQv. I	Jse calcula	ated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



Assume 80% of WQv treated

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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Subsurface Infiltration
Removal Efficiency:	100%
P Load>	13.10 lb/yr
	5.94 kg/yr
P Removal>	13.10 lb/yr
	5.94 kg/yr

Summary:

Proposed Retrofit Practice Subsurface Infiltration			
Drainage Area (acres)	3.0	Phosphorus Loading (kg/yr)	
Water Quality Volume (cf)	12415	Phosphorus Reduction (kg/yr)	4.75

4.75 kg/yr



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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-6 B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

## Kent-6 B: Kent Elementary & Primary Schools

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
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A =	2.7	acres	where:	A =	Contributing Area (acres)
1 =	2.5	92.59%		ł =	Impervious Area (acres/%)
P = 1.2		inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)	=	0.8833		WQv =	Water Quality Volume
Rv (min)** =		0.8833			
WQv (acre-ft)	=	0.239			
WQv (cu-ft) =		10389			
**Minimum Rv	= 0.	2 when determi	ning WQv.	Use calcula	ated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.8833		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.7		Rv =	Runoff Coefficient
C =	0.49		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.93
Develped Open Space	0.073
Weighted "C"	: 0.49



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter		
Removal Efficiency:	59%		
P Load>	10.67 lb/yr		
	4.84 kg/yr		
P Removal>	6.29 lb/yr		
	2.86 kg/yr		
	2.86 kg/yr		

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	2.7	Phosphorus Loading (kg/yr)	4.84
Water Quality Volume (cf)	10389	Phosphorus Reduction (kg/yr)	2.86







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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Kent-6C Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

## Kent-6C: Kent Elementary & Primary Schools

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	3.6	acres	where:	A =	Contributing Area (acres)
1 =	3.6	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)	=	0.9500		WQv =	Water Quality Volume
Rv (min)** =		0.9500			
WQv (acre-ft)	=	0.342			
WQv (cu-ft) =		14898			
**Minimum Rv	= 0.3	2 when determi	ning WQv. I	Use calcul	ated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3.6		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Surface Sand Filter
59%
15.72 lb/yr
7.13 kg/yr
9.28 lb/yr
4.21 kg/yr

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	3.6	Phosphorus Loading (kg/yr)	7.13
Water Quality Volume (cf)	14898	Phosphorus Reduction (kg/yr)	4.21





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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	L-4
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Westchester

## L-4: Lewisboro Elementary School

WATER Q	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Iv)(A)]/12
A =	3.9 2.4	acres 61.54%	where:	A =   =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.3	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcula WQv (acre WQv (cu-f	uted)= h-ft) = ht) =	0.6038 0.255 11113		WQv =	Water Quality Volume

#### WQv PEAK FLOW:

Based upon NYSDEC	Stormwater	Manual.	Appendix B-2
-------------------	------------	---------	--------------

Tc =	hours	Tc =	Time of Concentration (hours)
CN =	94	CN =	Curve Number
qu =	#NUM!	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	#NUMI CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.1	103
P =	48.6	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.6038		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	3.9		Rv =	Runoff Coefficient
C =	0.42		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.62
Develped Open Space	0.38
Weighted *C*	: 0.42



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	9.87 lb/yr
	4.48 kg/yr
P Removal>	5.82 lb/yr
	2.64 kg/yr

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	3.9	Phosphorus Loading (kg/yr)	4.48
Water Quality Volume (cf)	11113	Phosphorus Reduction (kg/yr)	2.64





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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	L-5
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Westchester

## L-5: Lewisboro Town Park

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	1.4	acres	where:	A =	Contributing Area (acres)
1 =	1.4	100.00%		1 =	Impervious Area (acres/%)
P =	1.3	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	(ated)=	0.9500		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.144			
WQv (cu	-ft) =	6276			

#### PHOSPHORUS LOADING:

Simple	Method:	PLoad = P x Pj x Rv x	CXAXO.	103
P =	48.6	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.4		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Subsurface Infiltration		
100%		
6.60 lb/yr		
3.00 kg/yr		
6.60 lb/yr		
3.00 kg/yr		

Proposed Retrofit Practice	Subsurface Infiltration		
Drainage Area (acres)	1.4	Phosphorus Loading (kg/yr)	3.00
Water Quality Volume (cf)	6276	Phosphorus Reduction (kg/yr)	3.00



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teboro Cense River	RENNIA ENGINEERING DESIGN, FILLO ON - ON FORMERTAL - TRACTIMENT OF A CONTORTING TO A CONTORTING OF A CONTORTANTI A CONTORTANTA CONTORTA CONTORTANTA CONTORTANTA CONTOP	Woodard & Curran Engineering PA PC 790 Westcheeter Averuu, Suite L2 White Platha, New York 19564 850,007,4330   www.woodardstaram.com	WOODARD COMPETE DACHBRRAM X77.DMD
E: 1° = 4000 Map SHOWN HEREON TAKEN FROM COUNTY TAX I OGRAPHIC INFORMATION SHOWN HEREON PF PARTMENT OF ENVIRONMENTAL PROTECTION 12, SUBJECT TO GIS DATA SHARING AGREEME DHWC. LAND INFO TAKEN FROM CORNELL UNIVERSIT TION REPOSITORY. INFORMATION SHOWN HEREON PROVIDED BY VCEPTUAL DESIGN PURPOSES ONLY. UES INCLUDED IN THIS RETROFIT PLAN ARE ED O AND SEALED PHOSPHORUS LOADING CALCU ORMED IN ACCORDANCE WITH THE EOHWC D WITH THE LATEST APPROVED NYSDEC "ALTER IN FORMULA". THE FINAL CALCULATIONS SHO CONFIRM CHANNEL DIMENSIONS, AND A COMI TATIONS OF ALL INPUT PARAMETERS USED IN 2 STABILIZATION FORMULA", INCLUDING THE	MAPPING, ROVIDED , BUREAU NT Y STIMATED LATIONS JESIGN NATIVE JULD PLETE THE BEHI AND	STORMWATER RETROFIT CONCEPT PLAN	DESIGNED BY: CRP/RGL CHECKED BY: LLP DESIGNED BY: CRP/RGL LEWSBOROLONOPONDPRESERVE.
ABILIZATION OF CLASSIFIED STREAM AND EXI ANNELS ON PRIVATE PROPERTIES, INCLUDING A-BIT DRIVE) HAS EXISTING ROADSIDE SWALE PES DISCHARGING TO LONG POND PRESERVE LY TO STREAM. SS TARRY-A-BIT DRIVE TO LONG POND PRESERVE TO REDUCE VOLUME OF RUNOFF DISCHARGIN NEW CROSSING INCLUDES A NEW CATCH BAS ILET STABILIZATION ON LONG POND PRESERV TARRY-A-BIT DRIVE, WHICH APPEARS TO BE C OUT OF PORTIONS OF THE GRAVEL ROAD, IS ACED.	STING S LONG S AND S RVE NG SIN INLET, /E AUSING	STREAM & CHANNEL STABILIZATION LONG POND PRESERVE	TOWN OF LEWISBORD
		JOB NO: DATE: By SCALE: 1 L-4	/12/16 *=100' 6

Channel ID	A	В	c	D	E	F
Channel Depth - y (ft)	4.0	2.0	3.0	4.0		
Channel Bottom Width - B (ft)	15.0	3.0	3.0	15.0		(
Channel Top Width -T (ft)	20.0	5.0	5.0	20.0		
Wetted Perimeter Calculation- P (ft)	24.43	7,47	9.32	24,43		
Channel Length-L (ft)	350	40	130	300		
Soil Erosion Depth-D (ft)	0.065	0.065	0.065	0.065		
Soil Erosion Volume-V (ft <sup>3</sup> )	555.9	19.4	78.8	476.5		
Weight* (lbs)	52,807.9	1,845.6	7,485.3	45,264.0		
Weight (Kg)	23,953.7	837.2	3,395.3	20,531.7		
P Load** (mg/Yr)	7,186,104.7	251,151.6	1,018,597.8	6,159,518.3		
P Load (Kg/Yr)	7.19	0.25	1.02	6.16		

ESTIMATED TOTAL (KG/YR): 14.62

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)







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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-1 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

## Pat-1: Big Elm Detention Pond

WATER QUALITY VOLUME: WQv(acre-feet) = [(P)(Rv)(A)] /12

A =	9	acres	where:	A =	Contributing Area (acres)
1 =	2.7	30.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated):	-	0.3200		WQv =	Water Quality Volume
Rv (min)** =		0.3200			
WQv (acre-ft)	=	0.288			
WQv (cu-ft) =		12545			
**Minimum Rv	= 0.	2 when determi	ning WQv. I	Use calcul	ated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3200		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	9		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	10.86 lb/yr
	4.92 kg/yr
P Removal>	5.97 lb/yr
	2.71 kg/yr

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	9.0	Phosphorus Loading (kg/yr)	4.92
Water Quality Volume (cf)	12545	Phosphorus Reduction (kg/yr)	2.71

PROPOSED STORMWATER RETROFIT PROJECT: **RETROFIT EXISTING DETENTION POND TO** PROVIDE WATER QUALITY TREATMENT (WET EXTENDED DETENTION POND)

> Clancy Properties L PO Box 291

> > **Clancy Relocation & Logistics**

EST, PHOSPHORUS REMOVAL: 4.14 KG/YR SEE ATTACHED CALCULATION SHEET

Letrofit Existing Detention Pond 33604 st

NYSEG.

Source: ArcGIS World Street Map PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING.

- **GENERAL NOTES:**
- TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY 2.
- SHARING AGREEMENT BETWEEN NYCDEP & EOHWC. NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL INFORMATION REPOSITORY.
- DESIGN PURPOSES ONLY.

#### SITE SPECIFIC NOTES:

- OWNER TO OBTAIN EASEMENTS FOR ANY WORK PERFORMED.
- BEING CAPTURED/TREATED BY THE PROPOSED SRP. OBTAIN AS-BUILT SURVEY INFORMATION OF EXISTING DETENTION POND AND SPECIFY NECESSARY MODIFICATIONS TO CONVERT TO WATER QUALITY POND
- δ. REQUIREMENTS ASSOCIATED WITH THE PROPOSED RETROFIT.







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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-2 East of Hudson Coalition Prepared for: Prepared by: CRP Project County: Putnam

## Pat-2: Clancy Relocation & Logistics

WATER O	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	7.6 7.6	acres 100.00%	where:	A =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = By =	90th Percentile Rainfall Event Number (in) Bunoff Coefficient [0.05 + 0.009(I)]
Rv = WQv (acr WQv (cu-	re-ft) = ft) =	0.9500 0.722 31450		WQv =	Water Quality Volume

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pi =	Fraction of rainfall producing Runoff = 0.9
A =	7.6		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond	
Removal Efficiency:	55%	
P Load>	33.19 lb/yr	
	15.05 kg/yr	
P Removal>	18.25 lb/yr	
	8.28 kg/yr	

4.14 kg/yr	Assume 50% of WQv treated
------------	---------------------------

Proposed Retrofit Practice	Wet ED Po	nd	
Drainage Area (acres)	7.6	Phosphorus Loading (kg/yr)	15.05
Water Quality Volume (cf)	31450	Phosphorus Reduction (kg/yr)	4.14







1:1

PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING. TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER SUPPLY, 2012, SUBJECT TO GIS DATA SHARING AGREEMENT BETWEEN NYCDEP &

NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL

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## PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-3 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

## Pat-3: Devon Road

WATER QUALITY VOLUME: WQv(acre-feet) = [(P)(Rv)(A)] /12

A =	14.5	acres	where:	A =	Contributing Area (acres)
1 =	2.6	17.93%		ł =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.2114		WQv =	Water Quality Volume
WQv (acre	-ft) =	0.307			
WQv (cu-fi	t) =	13351			
	-			and the second second second second	

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103				
P =	45	where:	P Load=	Annual load (kg/yr)		
Pj =	0.9		P =	Annual Rainfall (inches)		
Rv =	0.2114		Pi =	Fraction of rainfall producing Runoff = 0.9		
A =	14.5		Rv =	Runoff Coefficient		
C =	0.38		C =	Pollutant Concentration (mg/l)		
			A =	A = Contributing Area (acres)		

Land Use	% of Total Area
Residential	0.9
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0.1
Impervious	0
Develped Open Space	0
Weighted "C"	. 0.38



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond	
Removal Efficiency:	55%	
P Load>	10.82 lb/yr	
	4.91 kg/yr	
P Removal>	5.95 lb/yr	
	2.70 kg/yr	

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	14.5	Phosphorus Loading (kg/yr)	4.91	
Water Quality Volume (cf)	13351	Phosphorus Reduction (kg/yr)	2.70	






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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Pat-4
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Pat-4: Fox Run Condos

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	7.2	acres	where:	A =	Contributing Area (acres)
1 =	7.2	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.9500		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.684			
WOy (cu	-ft) =	29795			

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	7.2		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	31.44 lb/yr
	14.26 kg/yr
P Removal>	17.29 lb/yr
	7.84 kg/yr

6.28 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	7.2	Phosphorus Loading (kg/yr)	14.26
Water Quality Volume (cf)	29795	Phosphorus Reduction (kg/yr)	6.28



	1 I I I I I I I I I I I I I I I I I I I	DEEP TEST PIT RESULTS		
	TEST PIT	DEPTH FROM SURFACE(INCH)	SOIL DESCRIPTION	
D 'FAIR	TP-1	0" - 4"	TOPSOIL	
RK" PREPARED		4" - 36"	BROWN LOAMY SAND	
DISTURBED BY		36" - 84"+	MIXED SANDS WITH BROKEN ROCK / SHALE MIX	
, in the	TP-2	0" - 6"	TOPSOIL	
OF ANY		6" - 32"	BROWN LOAMY SAND	
		32" - 84"+	MIXED SANDS WITH BROKEN ROCK / SHALE MIX	

10/12/12

13.3 MIN/INCH

LEGEND

PERCOLATION TEST RESULTS PERCHOLE # PERCRATE

EXISTING 2' CONTOUR

/		

EXISTING 10' CONTOUR	
EXISTING SPOT GRADE	× 447.07
WETLAND BOUNDARY	
WETLAND FLAG	$\times$ WF A3
100' TOWN WETLAND BUFFER	
EXISTING TREE	0
EXISTING DRAINAGE PIPE	
EXISTING MONITORING WELL	Θ
EXISTING STONE WALL	-0000000000
PROPOSED 2' CONTOUR	446
PROPOSED 1' CONTOUR	
PROPOSED 10 CONTOUR	450
PROPOSED ASPHALT CURB	(j)
PROPOSED DRAINAGE PIPE	
PROPOSED HEADWALL WITH VELOCITY DISSIPATER	<b>C</b>
PROPOSED DRAINAGE MANHOLE	0
PROPOSED DRAIN INLET	
PROPOSED OUTLET STRUCTURE	
DEEP TEST HOLE LOCATION	<sup>TP 5</sup> �
PERCOLATION TEST HOLE LOCATION	PT 4
PROPOSED SILT FENCE	SFSF
TEMPORARY STONE CHECK DAMS	+++++++++++++++++++++++++++++++++++++++
PROPOSED TREE TO BE RMEOVED	8
PROPOSED TREE PROTECTION	0
PROPOSED LIMIT OF DISTURBANCE	

PROPOSED MAINTENANCE AND ACCESS EASEMENT

# NOT FOR CONSTRUCTION

KELLARD	STORMWA FAIR ST. &	TER MANAC	GEMENT PLAN RNER (MB-05)
CONSULTING	EOH STOI	WC CONTRAC <sup>®</sup> RMWATER RE	Г 2012 - 01 TROFITS
ENGINEERING.	TOWN OF PATTERSON		PUTNAM COUNTY, NEW YO
LANDSCAPE ARCHITECTURE		9,	0 /
PLANNING, P.C.		7.	/15
500 MAIN STREET		6. 5.	
ARMONK, N.Y. 10504		- <b>4</b> ,	PROJECT I.D.:
F: (914) 273-2323 F: (914) 273-2329		3. 2. FEBRUARY 1, 2013 - 90% 5	EHW100
WWW.KELSES.COM		1. JANUARY 22, 2013 - GENE REVISION	CRAL REVISIONS DATE: NOVEMBER 16,

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-5 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-5: Gottwald Property

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	25.7	acres	where:	A =	Contributing Area (acres)
1 =	5.91	23.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.2570		WQv =	Water Quality Volume
WQv (ac	re-ft) =	0.660			
WQv (cu	-ft) =	28767			

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.2570		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	25.7		Rv =	Runoff Coefficient
C =	0.43		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0.77
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.23
Develped Open Space	0
Weighted "C"	0.43



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond	
Removal Efficiency:	67%	
P Load>	26.15 lb/yr	
	11.86 kg/yr	
P Removal>	17.52 lb/yr	
	7.95 kg/yr	

5.92 kg/yr	Assume 80%	of WQv treated
------------	------------	----------------

Proposed Retrofit Practice	Pocket Pond			
Drainage Area (acres)	25.7	Phosphorus Loading (kg/yr)	11.86	
Water Quality Volume (cf)	28767	Phosphorus Reduction (kg/yr)	5.92	





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-6 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-6: Indian Hill Road

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Tv)(A)]/12
A =	57.4	acres	where:	A =	Contributing Area (acres)
1 =	8.2	14.29%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.1786		WQv =	Water Quality Volume
WQv (ac	re-ft) =	1.025			
WQv (cu	-ft) =	44649			

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.1786		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	57.4		Rv =	Runoff Coefficient	
C =	0.30		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0.59
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0.41
Impervious	0
Develped Open Space	0
Weighted "C":	0.30



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond		
Removal Efficiency:	55%		
P Load>	28.59 lb/yr		
	12.97 kg/yr		
P Removal>	15.72 lb/yr		
	7.13 kg/yr		

5.71 kg/yr A	ssume 80% of WQv treated
--------------	--------------------------

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	57.4	Phosphorus Loading (kg/yr)	12.97	
Water Quality Volume (cf)	44649	Phosphorus Reduction (kg/yr)	5.71	







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-7 Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-7: JRS Pharma

WATER QUALITY VOLUME: WQv(acre-feet) = [(P)(Rv)(A)]/12

A =	3.8	acres	where:	A =	Contributing Area (acres)
1 =	3.8	100.00%		ł =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.9500		WQv =	Water Quality Volume
WQv (acre-	-ft) =	0.361			
WQv (cu-ft	) =	15725			
		A	1110	Income and the second	A CONTRACT OF A CO

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103		
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pi =	Fraction of rainfall producing Runoff = 0.9
A =	3.8		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Subsurface Infiltration
Removal Efficiency:	100%
P Load>	16.59 lb/yr
	7.53 kg/yr
P Removal>	16.59 lb/yr
	7.53 kg/yr

6.02 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Subsurface Infiltration			
Drainage Area (acres)	3.8	Phosphorus Loading (kg/yr)	7.53	
Water Quality Volume (cf)	15725	Phosphorus Reduction (kg/yr)	6.02	





Image: State of Basin         Catch Basin		Woodard & Currer Engineering PA PC 700 Westcheeen Arenva, Suite L2 White Pfalms, Now York 19664 850.607.4380   www.woodandstremn.com	WOODARD COMMITMENT & INTEGRITY DRIVE RESULTS
TAKEN FROM COUNTY TAX MAPPING. MATION SHOWN HEREON PROVIDED BY NEW ENTAL PROTECTION, BUREAU OF WATER SUPPLY, BREEMENT BETWEEN NYCOEP & COHWO. I FROM CORNELL UNIVERSITY GEOSPATIAL DWN HEREON PROVIDED BY MUNICIPALITY FOR D AS AN ESTIMATE FOR CONCEPTUAL USE ONLY, ATCHMENT BOUNDARIES MUST BE COMPLETED PROPERTY AND WILL REQUIRE COORDINATION I EASEMENTS FOR ANY WORK PERFORMED, IN AND CONTAINS EXISTING DETENTION POND OF EXISTING DETENTION POND AND SPECIFY TO UNITED OUNDARIES DUDY	t Branch Catch Basin Catch Basin Catch Basin	STORMWATER RETROFIT CONCEPT PLAN	DESIGNED BY: CRP/RGL CHECKED BY: LLP DRAWN BY: CRP/RGL MANORROAD_CONCEPTSKETCHB_FID
AND CONTAINS EXISTING DETENTION POND OF EXISTING DETENTION POND AND SPECIFY OF EXISTING DETENTION POND AND SPECIFY	TAKEN FROM COUNTY TAX MAPPING. MATION SHOWN HEREON PROVIDED BY NEW SITAL PROTECTION, BUREAU OF WATER SUPPLY, BREEMENT BETWEEN NYCOEP & EOHWC. I FROM CORNELL UNIVERSITY GEOSPATIAL OWN HEREON PROVIDED BY MUNICIPALITY FOR	RETROFIT EXISTING DETENTION POND MANOR ROAD - B	TOWN OF PATTERSON
PAT-6B	LEASEMENTS FOR ANY WORK PERFORMED, IN AND CONTAINS EXISTING DETENTION POND OF EXISTING DETENTION POND AND SPECIFY RT TO WATER QUALITY POND.	JOB NO: DATE: 8/ SCALE: 1 PAT-	/12/16 1*60' -6B

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-8 A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-8 A: Manor Road

WATER	QUALITY VOLUME	: WQv(acre-fee	WQv(acre-feet) = [(P)(Rv)(A)]/12		
A =	4.4 acres	where:	A =	Contributing Area (acres)	
10110	10 07 070/		1	Importánia Aron (aprop/0)	

1=	1.2	27.27%	1 =	Impervious Area (acres/%)
P =	1.2	inches	P =	90th Percentile Rainfall Event Number (in)
			Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.2955	WQv =	Water Quality Volume
WQv (acre-fi	t) =	0.130		
WQv (cu-ft)	=	5663		

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.2955		Pi =	Fraction of rainfall producing Runoff = 0.9
A =	4.4		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C":	0.41



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	4.90 lb/yr
	2.22 kg/yr
P Removal>	2.70 lb/yr
	1.22 kg/yr

Proposed Retrofit Practice	Wet ED Pond		
Drainage Area (acres)	4.4	Phosphorus Loading (kg/yr)	2.22
Water Quality Volume (cf)	5663	Phosphorus Reduction (kg/yr)	1.22



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-8 B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-8 B: Manor Road

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12

A =	11.8	acres	where:	A =	Contributing Area (acres)
1 =	3.6	30.51%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.3246		WQv =	Water Quality Volume
WQv (acre-	-ft) =	0.383			
WQv (cu-ft	) =	16683			
and distances	D. 0	O ush an data and	alar Michael I	Terrer and terrer	at a difference of a second a local second a local second s

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

#### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3246		Pi =	Fraction of rainfall producing Runoff = 0.9
A =	11.8		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	14.44 lb/yr
	6.55 kg/yr
P Removal>	7.94 lb/yr
	3.60 kg/yr

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	11.8	11.8 Phosphorus Loading (kg/yr)		
Water Quality Volume (cf)	16683	Phosphorus Reduction (kg/yr)	3.60	





PAT-9A

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PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX

Putners Lake - D/D

Putnert Lake -B

Arran Lake A

Dayton Rel

TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER SUPPLY, 2012, SUBJECT TO GIS DATA SHARING AGREEMENT BETWEEN NYCDEP & EOHWC. NEW YORK STATE WETLAND INFO TAKEN FROM CORNELL UNIVERSITY GEOSPATIAL INFORMATION REPOSITORY. ANY EXISTING UTILITY INFORMATION SHOWN HEREON PROVIDED BY MUNICIPALITY FOR CONCEPTUAL DESIGN PURPOSES ONLY.

DRAINAGE AREA INDICATED IS INTENDED AS AN ESTIMATE FOR CONCEPTUAL USE ONLY, FURTHER EVALUATION OF ACTUAL SUBCATCHMENT BOUNDARIES MUST BE COMPLETED AS PART OF

PROPOSED SRP IS LOCATED ON PUTNAM LAKE COMMUNITY COUNCIL PROPERTY. COORDINATION WITH THE PROPERTY WILL BE REQUIRED TO OBTAIN EASEMENTS FOR ANY WORK PERFORMED. PROPOSED FILTERING PRACTICE AT END OF PIPE, EXISTING STORMWATER OUTFALL LOCATED IN AREA OF PROPOSED SRP. WHERE POSSIBLE, CONSIDERATION SHOULD BE GIVEN TO COMBINING MULTIPLE SRP's TO A SINGLE PRACTICE WHERE PROXIMITY OF OUTFALLS, EXISTING DRAINAGE INFRASTRUCTURE

STABILIZATION/ELIMINATION OF EXISTING ERODED CHANNELS BETWEEN OUTFALL DISCHARGE AND LAKE CARMEL SHOULD BE











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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Pat-9 A
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Pat-9 A: Putnam Lake

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	(v)(A)]/12
A = I = P = Rv (cak WQv (a WQv (c	5.2 1.6 1.2 culated)= ccre-ft) = cu-ft) =	acres 30.77% inches 0.3269 0.170 7405	where:	A = I = P = Rv = WQv =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQV PE	AK FLOW:				
Based u	Ipon NYSD	EC Stormwa	iter Manual. App	pendix B-2	
Tc =	0.15	hours		Tc =	Time of Concentration (hours)
CN =	88			CN =	Curve Number
qu =	607.249			qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	1.93561	CFS		Qp =	Peak Discharge (CFS)
PHOSP	HORUSLO	DADING:			
Simple	Method:	P Load	= P x Pj x Rv x	CXAX0.	103
P =	45		where:	P Load=	Annual load (kg/yr)
Pj =	0.9			P =	Annual Rainfall (inches)
Rv =	0.3269			Pj =	Fraction of rainfall producing Runoff = 0.9
A =	5.2			Rv =	Runoff Coefficient
C =	0.41			C =	Pollutant Concentration (mg/l)
				A =	A = Contributing Area (acres)

% of Total Area
1
0
0
0
0
0
0
0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Stormfilter
Removal Efficiency:	40%
P Load>	6.41 lb/yr
	2.91 kg/yr
P Removal>	2.56 lb/yr
	1.16 kg/yr

Proposed Retrofit Practice	Stormfilter				
Drainage Area (acres)	5.2 Phosphorus Loading (kg/yr		2.91		
Water Quality Volume (cf)	7405	Phosphorus Reduction (kg/yr)	1.16		



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Pat-9 B
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Pat-9 B: Putnam Lake

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	(v)(A)]/12
A = I = P = Rv (cak WQv (a WQv (c	29.2 9 1.2 culated)= icre-ft) = cu-ft) =	acres 30.82% inches 0.3274 0.956 41643	where:	A = I = P = Rv = WQv =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQv PE/	AK FLOW:	FO 64			
based u	Ipon INTSU	EC Stormwa	ter Manual. App	pendix B-2	물날 방법 - 김 정 김
Tc =	0.25	hours		Tc =	Time of Concentration (hours)
CN =	88			CN =	Curve Number
qu =	513.485			qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	9.20421	CFS		Qp =	Peak Discharge (CFS)
PHOSP	HORUSLO	DADING:			
Simple	Method:	P Load	= P x Pi x Rv x	CXAX0.	103
P =	45		where:	P Load=	Annual load (kg/vr)
Pi =	0.9			P =	Annual Rainfall (inches)
Rv =	0.3274			Pi =	Fraction of rainfall producing Runoff = 0.9
A =	29.2			Ry =	Runoff Coefficient
C =	0.41			C =	Pollutant Concentration (mg/l)
973Ge				A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	: 0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Stormfilter
40%
36.03 lb/yr
16.35 kg/yr
14.41 lb/yr
6.54 kg/yr

5.23 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter			
Drainage Area (acres)	29.2	Phosphorus Loading (kg/yr)	16.35	
Water Quality Volume (cf)	41643	Phosphorus Reduction (kg/yr)	5.23	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	Pat-9 C/D
Prepared for:	East of Hudson Coalition
Prepared by:	CRP
Project County:	Putnam

# Pat-9 C/D: Putnam Lake

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	v)(A)]/12
A = I = P = <b>Rv</b> (calc	91 23 1.2 :ulated)=	acres 25.27% inches 0.2775	where:	A = I = P = Rv = WQv =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQv (a WQv (c WQv PEA	cre-ft) = u-ft) = NK FLOW:	2.525			
Based u	Ipon NYSU	EC Stormwa	ter Manual. App	bendix B-2	
TC =	1.2	hours		TC =	Time of Concentration (hours)
CN =	87			CN =	Curve Number
qu =	243.737			qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	11.5394	CFS		Qp =	Peak Discharge (CFS)
PHOSP	HORUS LO	DADING:			
Simple	Method:	P Load	= P x Pj x Rv x	CXAXO.	103
P =	45		where:	P Load=	Annual load (kg/yr)
Pj =	0.9			P =	Annual Rainfall (inches)
Rv =	0.2775			Pj =	Fraction of rainfall producing Runoff = 0.9
A =	91			Rv =	Runoff Coefficient
C =	0.41			C =	Pollutant Concentration (mg/l)
				A =	A = Contributing Area (acres)

% of Total Area
1
0
0
0
0
0
0
0.41



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Stormfilter
40%
95.18 lb/yr
43.17 kg/yr
38.07 lb/yr
17.27 kg/yr

13.81 kg/yr Assume 80% of WQv treated

Proposed Retrofit Practice	Stormfilter				
Drainage Area (acres)	91.0	Phosphorus Loading (kg/yr)	43.17		
Water Quality Volume (cf)	109989	Phosphorus Reduction (kg/yr)	13.81		





1:1










#### LOCATION MAP: SCALE: 1" = 6000"

Source: ArcGIS World Street Map

Fise

Big Elm Detention Pond - A

#### **GENERAL NOTES:**

- PARCEL INFORMATION SHOWN HEREON TAKEN FROM COUNTY TAX MAPPING. TOPOGRAPHIC & HYDROGRAPHIC INFORMATION SHOWN HEREON PROVIDED BY NEW YORK CITY DEPARTMENT OF ENVIRONMENTAL PROTECTION, BUREAU OF WATER
- SUPPLY, 2012, SUBJECT TO GRIS DATA SHARING AGREEMENT BETWEEN NYCDEP & EOHWC. 3. NEW YORK BTATE WETLAND INFO
- INFORMATION REPOSITORY.
- ANY EXISTING UTILITY INFORMATION SHOWN HEREON PROVIDED
- CONCEPTUAL DESIGN PURPOSES ONLY, DRAINAGE AREA INDICATED IS INTENDED AS AN ESTIMATE FOR CONCEPTUAL USE ONLY, FURTHER EVALUATION OF ACTUAL SUBCATCHMENT BOUNDARIES MUST BE COMPLETED AS PART OF DETAILED DESIGN. 5.





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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-10 A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-10 A: Robin Hill Corporate Park

A =	15.29	acres	where:	A =	Contributing Area (acres)
1 =	6.3	41.20%		ł =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculat	ed)=	0.4208		WQv =	Water Quality Volume
Rv (min)** =		0.4208			
WQv (acre-	ft) =	0.643			
WQv (cu-ft	) =	28029			
**Minimum	Rv = 0.3	2 when determi	ining WQv. I	Use calcul	ated Rv when determining phosphorus loading.

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAxO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.4208		Pi=	Fraction of rainfall producing Runoff = 0.9
A =	15.29		Rv =	Runoff Coefficient
C =	0.47		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0.59
Actively Grazed Pasture	0
Forest	0
Impervious	0.41
Develped Open Space	0
Weighted *C	: 0.47



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	27.83 lb/yr
	12.62 kg/yr
P Removal>	15.31 lb/yr
	6.94 kg/yr

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	15.3 Phosphorus Loading (kg/yr)		12.62	
Water Quality Volume (cf)	28029	Phosphorus Reduction (kg/yr)	6.94	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-10 B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-10 B: Robin Hill Corporate Park

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	1.6	acres	where:	A =	Contributing Area (acres)
1 =	1.6	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)=		0.9500		WQv =	Water Quality Volume
Rv (min)** =		0.9500			
WQv (acre-ft) :	=	0.152			
WQv (cu-ft) =		6621			
**Minimum Rv	= 0.2	2 when determi	ning WQv. I	Use calcula	ated Rv when determining phosphorus loading.

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.6		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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# PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	6.99 lb/yr
	3.17 kg/yr
P Removal>	4.68 lb/yr
	2.12 kg/yr

Proposed Retrofit Practice	Pocket Pond			
Drainage Area (acres)	1.6 Phosphorus Loading (kg/yr)			
Water Quality Volume (cf)	6621	Phosphorus Reduction (kg/yr)	2.12	



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-10 C Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-10 C: Robin Hill Corporate Park

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)] /12
-----------------------	-----------------------------------

A =	1.7	acres	where:	A =	Contributing Area (acres)
1 =	1.7	100.00%		ł =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)	=	0.9500		WQv =	Water Quality Volume
Rv (min)** =		0.9500			
WQv (acre-ft)	=	0.162			
WQv (cu-ft) =		7035			
**Minimum Rv	= 0.3	2 when determi	ning WQv. I	Use calcula	ated Rv when determining phosphorus loading.

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.7		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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# PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	7.42 lb/yr
	3.37 kg/yr
P Removal>	4.97 lb/yr
	2.26 kg/yr

Proposed Retrofit Practice	Pocket Pond				
Drainage Area (acres)	1.7	Phosphorus Loading (kg/yr)	3.37		
Water Quality Volume (cf)	7035	Phosphorus Reduction (kg/yr)	2.26		



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-10 D Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-10 D: Robin Hill Corporate Park

WATER QUALITY VOLUME: WQv(acre-fee	set,	) =	: [(F	P)(R	v)(A	)]/1	2	
------------------------------------	------	-----	-------	------	------	------	---	--

A =	2.8	acres	where:	A =	Contributing Area (acres)
1 =	2.8	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)	=	0.9500		WQv =	Water Quality Volume
Rv (min)** =		0.9500			
WQv (acre-ft)	=	0.266			
WQv (cu-ft) =		11587			
**Minimum Rv	= 0.3	2 when determi	ning WQv. I	Use calcul	ated Rv when determining phosphorus loading.

# PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.8		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C"	: 0.50



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	12.23 lb/yr
	5.55 kg/yr
P Removal>	8.19 lb/yr
	3.72 kg/yr

Proposed Retrofit Practice	Pocket Pond				
Drainage Area (acres)	2.8	5.55			
Water Quality Volume (cf)	11587	Phosphorus Reduction (kg/yr)	3.72		



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-10 E Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-10 E: Robin Hill Corporate Park

A =	6.94	acres	where:	A =	Contributing Area (acres)
1 =	2.94	42.36%		ł =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculat	ed)=	0.4313		WQv =	Water Quality Volume
Rv (min)** =		0.4313			
WQv (acre-	-ft) =	0.299			
WQv (cu-ft	) =	13038			
**Minimum	Rv = 0.	2 when determi	ning WQv. I	Jse calcul	ated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.4313		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	6.94		Rv =	Runoff Coefficient
C =	0.30		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0.58
Impervious	0.42
Develped Open Space	0
Weighted "C"	: 0.30



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# PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	8.17 lb/yr
	3.71 kg/yr
P Removal>	5.48 lb/yr
	2.48 kg/yr

Proposed Retrofit Practice	Pocket Pond			
Drainage Area (acres)	6.9 Phosphorus Loading (kg/yr)		3.71	
Water Quality Volume (cf)	13038	Phosphorus Reduction (kg/yr)	2.48	







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-11 A Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-11 A: Watchtower

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	8.93	acres	where:	A =	Contributing Area (acres)
=	6.23	69.76%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.6779		WQv =	Water Quality Volume
WQv (acre-ft) = 0.605					
WOv (cu-ft) = 26369					

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAXO.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.6779		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	8.93		Rv =	Runoff Coefficient
C =	0.44		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.7
Develped Open Space	0.3
Weighted "C":	0.44



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## PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	24.40 lb/yr
	11.07 kg/yr
P Removal>	13.42 lb/yr
	6.09 kg/yr

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	8.9 Phosphorus Loading (kg/yr)			
Water Quality Volume (cf)	26369	Phosphorus Reduction (kg/yr)	6.09	







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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-11 B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-11 B: Watchtower

WATER (	UALITY	VOLUME:	WQv(acre-fee	et) = [(P)(P)	Rv)(A)]/12
A =	2.9	acres	where:	A =	Contributing Area (acres)
1 =	2.9	100.00%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.9500		WQv =	Water Quality Volume
WQv (acre-ft) = 0.276					
W/0v /ou-#1 = 12001					

\*\*Minimum Rv = 0.2 when determining WQv. Use calculated Rv when determining phosphorus loading.

### PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CxAx0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.9500		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.9		Rv =	Runoff Coefficient
C =	0.50		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	1
Develped Open Space	0
Weighted "C":	0.50



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# PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Wet ED Pond
Removal Efficiency:	55%
P Load>	12.66 lb/yr
	5.74 kg/yr
P Removal>	6.97 lb/yr
	3.16 kg/yr

Proposed Retrofit Practice	Wet ED Pond			
Drainage Area (acres)	2.9 Phosphorus Loading (kg/yr)		5.74	
Water Quality Volume (cf)	12001	Phosphorus Reduction (kg/yr)	3.16	





Channel ID	A	в	C	D	E	F
Channel Depth - y (#)	7.0	3.5	4.5			
Channel Bottom Width - B (ft)	25.0	8.0	6.0			
Channel Top Width -T (ft)	30.0	12.0	10.0			
Vetted Perimeter Calculation- P (ft)	39.87	16.06	15.85			
Channel Length-L (ft)	570	220	230	ļ		
Soil Erosion Depth-D (ft)	0.065	0.065	0.065			
Soil Erosion Volume-V (It <sup>3</sup> )	1,477.0	229.7	236.9			
Weight* (lbs)	140,318.6	21,820.6	22,509.3			а 1
Weight (Kg)	63,648.5	9,897.8	10,210.2			
P Load** (mg/Yr)	19,094,554.5	2,969,344.1	3,063,071.0			
P Load (Kg/Yr)	19.09	2.97	3.06			

ESTIMATED TOTAL (KG/YR): 25.13

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: Pat-12B Prepared for: East of Hudson Coalition Prepared by: CRP Project County: Putnam

# Pat-12B: CT Stream - B

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)] /12
-----------------------	-----------------------------------

A =	96.4	acres	where:	A =	Contributing Area (acres)
1 =	28.5	29.56%		1 =	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv =		0.3161		WQv =	Water Quality Volume
WQv (ac	re-ft) =	3.047			
WQv (cu	-ft) =	132727			

# PHOSPHORUS LOADING:

Simple	Method:	P Load = P x Pj x Rv x	CXAX0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3161		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	96.4		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

ï

Land Use	% of Total Area
Residential	1/
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0
Develped Open Space	0
Weighted "C"	0.41



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Multiple Pond
Removal Efficiency:	76%
P Load>	114.85 lb/yr
	52.10 kg/yr
P Removal>	87.29 lb/yr
	39.59 kg/yr

19.80 kg/yr A	ssume 50% of	WQv treated
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Proposed Retrofit Practice	Multiple Pond				
Drainage Area (acres)	96.4	6.4 Phosphorus Loading (kg/yr)			
Water Quality Volume (cf)	132727	Phosphorus Reduction (kg/yr)	19.80		



Channel ID	A	в	c	D	E	F
Channel Depth - y (ft)	5.0	8.0				
Channel Bottom Width - B (ft)	15.0	25.0				
Channel Top Width -T (ft)	20.0	30.0				
Vetted Perimeter Calculation- P (ft)	26.18	41.76	2			
Channel Length-L (ft)	130	250				
Soil Erosion Depth-D (ft)	0.065	0.065				
Soil Erosion Volume-V (ft <sup>3</sup> )	221.2	678.6				
Weight* (lbs)	21,016.3	64,471.7				- 
Weight (Kg)	9,533.0	29,244.4				
P Load** (mg/Yr)	2,859,893.7	8,773,311.1				
P Load (Kg/Yr)	2.86	8.77				

ESTIMATED TOTAL (KG/YR): 11.63

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EDHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

 Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wotted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soll Erosion Volume: V= P\*L\*D 8D\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

EST. PHOSPHORUS REMOVAL: 0.25 KG/R SEE ATTACHED CALCULATION SHEET BOODSED STORWATER RETROFIT PRACTICE CHANNEL STABILIZATION *80 LINEAR FEET	
PRACTICE AR	EA
LOCAL MAPPI WETLAND ARE	.D .A
MAPPED WATERCOURS	Ξ
GENERAL NOIES   1. SITE ORTHOIMAGERY, TOPOGRAPHY AND PROPERTY DATA OBTAINED FROM WESTCHESTER COUNTY DEPARTMENT OF PLANNING GEOGRAPHIC INFORMATION SYSTEMS INTERACTIVE MAPPER, JULY 2016.   2. STORM SEWER INFRASTRUCTURE REPRESENTED ON MAP AS APPROXIMATE BASED UPON PROVIDED MUNICIPAL GIS	
DATA. 3. CHANNEL STABILIZATION PROJECTS PROPOSED WITHIN CLASSIFIED STREAMS REQUIRE CASE BY CASE REVIEW AND	
APPROVAL BY NYSDEC, AS WELL AS APPROVAL OF THE PROPOSED STABILIZATION METHOD.	PIPE
APPROVAL BY NYSDEC, AS WELL AS APPROVAL OF THE PROPOSED STABILIZATION METHOD. 4. THE PHOSPHORUS VALUES INCLUDED ON THIS RETROFIT PLAN ARE ESTIMATED VALUES. FINAL SIGNED AND SEALED PHOSPHORUS LOADING CALCULATIONS WILL NEED TO BE PERFORMED IN ACCORDANCE WITH THE EOHWC DESIGN MANUAL CONSISTENT WITH THE LATEST APPROVED NYSDEC "ALTERNATIVE CHANNEL STABILIZATION FORMULA". THE FINAL CALCULATIONS SHOULD INCLUDE SURVEYS TO CONFIRM CHANNEL DIMENSIONS. AND A COMPLETE ANALYSIS AND NOT FOR CONSTRUCT	r PIPE [ <b>ON</b>
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PR-1_Ambler Way_Trapezoidal Channel Stabilization P-Loading Calculation	
Channel ID	A
Channel Depth - y (ft)	1.0
Channel Bottom Width - B (ft)	1.5
Channel Top Width -T (ft)	2.5
Wetted Perimeter Calculation-P (ft)	3.74
Channel Length-L (ft)	80
Soil Erosion Depth-D (ft)	0.065
Soil Erosion Volume-V (ft <sup>3</sup> )	19.4
Weight* (lbs)	1,845.6
Weight (Kg)	837.2
P Load** (mg/Yr)	251,151.6
P Load (Kg/Yr)	0.25
ESTIMATED TOTAL (KG/YR):	0.25

#### Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wetted Perimeter (P) approximately:  $P = T + [(8/3)^* (\gamma^2/T)]$ Soil Erosion Volume:  $V = P^*L^*D$ BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)



PR-3_Parkview Drive_Trapezoidal Channel Stabilization P-Loading Calculation	
Channel ID	A
Channel Depth - y (ft)	1.5
Channel Bottom Width - B (ft)	2.0
Channel Top Width -T (ft)	3.5
Wetted Perimeter Calculation-P (ft)	5.35
Channel Length-L (ft)	310
Soil Erosion Depth-D (ft)	0.065
Soil Erosion Volume-V (ft <sup>3</sup> )	107.9
Weight* (lbs)	10,249.1
Weight (Kg)	4,649.0
P Load** (mg/Yr)	1,394,696.1
P Load (Kg/Yr)	1.39
ESTIMATED TOTAL (KG/YR):	1.39

Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

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		PER POAD	
	EST. PHOSPHORUS REM SEE ATTACHED CALCUL	DPOSED STORMWATER ROFIT PRACTICE NNEL STABILIZATION to LINEAR FEET MOVAL: 2.31 KG/YR ATION SHEET	D CEPTUAL D
SITE SPECIFIC NOTES			CAL MAPPED LAND AREA
GENERAL NOTES 1. SITE ORTHOIMAGERY, TOPOGRAPHY AND PROPER PLANNING GEOGRAPHIC INFORMATION SYSTEMS 2. STORM SEWER INFRASTRUCTURE REPRESENTED DATA.	NICE AL BOUNDART OF POUND RIDGE. (TOWN OF LEV RTY DATA OBTAINED FROM WESTCHESTER COUNTY DI INTERACTIVE MAPPER, JULY 2016. ON MAP AS APPROXIMATE BASED UPON PROVIDED N	EPARTMENT OF AUNICIPAL GIS	IERCOURSE IRM SEWER CHARGE POINT
3. CHANNEL STABILIZATION PROJECTS PROPOSED APPROVAL BY NYSDEC, AS WELL AS APPROVAL 4. THE PHOSPHORUS VALUES INCLUDED ON THIS F PHOSPHORUS LOADING CALCULATIONS WILL NEE MANUAL CONSISTENT WITH THE LATEST APPROV FINAL CALCULATIONS SHOULD INCLUDE SURVEY COMPUTATIONS OF ALL INPUT PARAMETERS USI THE BEHI AND NBS INDEXES REINING ENGINEERING DESIGN, THE PAGGE	WITHIN CLASSIFIED STREAMS REQUIRE CASE BY CASE . OF THE PROPOSED STABILIZATION METHOD. RETROFIT PLAN ARE ESTIMATED VALUES. FINAL SIGNE D TO BE PERFORMED IN ACCORDANCE WITH THE EO VED NYSDEC "ALTERNATIVE CHANNEL STABILIZATION S TO CONFIRM CHANNEL DIMENSIONS, AND A COMPLI ED IN THE "ALTERNATIVE CHANNEL STABILIZATION FO BAR SCALE	E REVIEW AND STO ED AND SEALED HWC DESIGN FORMULA". THE ETE ANALYSIS AND RMULA", INCLUDING ANY ALTERATION OF PLAN PLATS AND REPORTS BEAR LICENSED PROFESSIONAL E LICENSED PROFESSIONAL E LICENSED PROFESSIONAL E LICENSED PROFESSIONAL E FDI/CATION LAW EVENT	RM SEWER PIPE STRUCTION S, SPECIFICATIONS, NING THE SEAL OF A NGINEER OR IS A VIOLATION OF W YORK STATE S PROVIDED FOR BY
Woodarn & Curran Engineering PA PC 709 Westchester Avenue, Suite L2 White Plains, New York 10604 800.807.4080   www.woodardcurran.com COMMITMENT & INTEGRITY DRIVE RESULTS	CHECK GRAPHIC SCALE BEFORE USING STORMWATER RETROFIT CONCEPT PLAN DESIGNED BY: RPW CHECKED BY: SL	CHANNEL STABILIZATION 26 DINGEE ROAD TOWN OF POUND RIDGE	JOB NO: 214336     DATE:   08/05/2016     SCALE:   AS SHOWN     PR-4

PR-4_Dingee Road_Trapezoidal Channel Stabilization P-Loading Calculation	
Channel ID	А
Channel Depth - y (ft)	2.0
Channel Bottom Width - B (ft)	7.0
Channel Top Width -T (ft)	9.0
Wetted Perimeter Calculation-P (ft)	11.47
Channel Length-L (ft)	240
Soil Erosion Depth-D (ft)	0.065
Soil Erosion Volume-V (ft <sup>3</sup> )	179.0
Weight* (lbs)	17,001.7
Weight (Kg)	7,712.0
P Load** (mg/Yr)	2,313,592.1
P Load (Kg/Yr)	2.31
ESTIMATED TOTAL (KG/YR):	2.31

Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis: Wetted Perimeter (P) approximately:  $P = T + [(8/3)^* (\gamma^2/T)]$ Soil Erosion Volume:  $V = P^*L^*D$ BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)



PC-1 - Stagecoach Road Trapezoidal Channel Stabilization P-Loading Calculation	
Channel ID	A
Channel Depth - y (ft)	2.5
Channel Bottom Width - B (ft)	3.0
Channel Top Width -T (ft)	5.0
Wetted Perimeter Calculation-P (ft)	8.39
Channel Length-L (ft)	320
Soil Erosion Depth-D (ft)	0.065
Soil Erosion Volume-V (ft <sup>3</sup> )	174.4
Weight* (lbs)	16,569.1
Weight (Kg)	7,515.7
P Load** (mg/Yr)	2,254,721.2
P Load (Kg/Yr)	2.25
ESTIMATED TOTAL (KG/YR):	2.25

Notes:

1. Channel dimensions are based upon field measurements taken by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

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Equation and Input Paramaters Basis: Wetted Perimeter (P) approximately:  $P=T+[(8/3)*(\gamma^2/T)]$ Soil Erosion Volume: V=P\*L\*DBD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)




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6 Dover Willige Places, Suite S. P.O. Ben 400, Dover Places, MY 12522 Tat. (545) 677-1565 Fax, (346) 677-1550



# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	PC-2
Prepared for:	EOHC
Prepared by:	RB/SL
Project County:	Putnam

# PC-2 - Putnam County Sheriff's Facility

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	v)(A)] /12
A = I = P =	8 5.6 1.2	acres 70.00% inches	where:	A = I = P =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in)
<b>Rv</b> (calcu <b>Rv</b> (min) <sup>*</sup> <b>WQv (ac</b>	ulated)= ** <b>=</b> : <b>re-ft)</b> =	0.6800 0.6800 <b>0.544</b>		Rv = WQv =	Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQv (cu **Minimu	<i>i-ft) =</i> im Rv = 0.3	23697 2 when deterr	nining WQv.	Use calcula	ted Rv when determining phosphorus loading.

### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.33 hou	irs .	Tc =	Time of Concentration (hours)
CN =	96	(	CN =	Curve Number
qu =	472.223		qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	4.81668 CFS	S (	Qp =	Peak Discharge (CFS)

## PHOSPHORUS LOADING:

Simple	Method:	P Load = P x P j x R v x	C x A x 0.1	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.6800		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	8		Rv =	Runoff Coefficient
C =	0.45		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	Fraction of 1	<b>Fotal Area</b>
Residential	0.0%	
Commercial	30.0%	
Industrial	0.0%	
Actively Grazed Pasture	0.0%	
Forest	0.0%	
Impervious	70.0%	
Develped Open Space	0.0%	
Weighted "C":	0.45	



6 Dover Wilege Places, Suite S. P.O. Box 400, Dover Places, MY 12522 Tail (245) 617-0565 Fax: (246) 677-0550



### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	StormFilter	
Removal Efficiency:	40%	
P Load>	22.61 lb/yr	
	<b>10.25</b> kg/yr	
P Removal>	<b>9.04</b> lb/yr	
	<b>4.10</b> kg/yr	

### Summary:

Proposed Retrofit Practice	StormFilter		
Drainage Area (acres)	8.0	Phosphorus Loading (kg/yr)	10.25
Water Quality Volume (cf)	23697	Phosphorus Reduction (kg/yr)	4.10





0	75	150	225	300	5.
				Feet	Legend
RENNIA		ING DESIGN		ACCI	Parcels
6 Dover Village Pla: Tel: (845) 877-0555	IENTAL • STRUCTURAL za, Suite 5, P.O. Box 400, Dove 5 Fax: (845) 877-0556	r Plains, NY 12522	ENK	SINEERING	+++ Propose
		STORMW			

COMMITMENT & INTEGRITY DRIV

- MAP SOURCE OBTAINED FROM ARCGIS WORLD IMAGERY SITE TOPOGRAPHY (2012) AND IMPERVIOUS AREA (2013) OBTAINED FROM NYCDEP PROPERTY DATA AND STORM SEWER INFRASTRUCTURE OBTAINED FROM VILLAGE OF BREWSTER CHANNEL STABILIZATION PROJECTS PROPOSED WITHIN CLASSIFIED STREAMS REQUIRE CASE BY CASE REVIEW AND APPROVAL BY NYSDEC, AS WELL AS AN APPROVAL OF THE PROPOSED 4.
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NEERING	Proposed	SRP Location		
A PC 2	STORMWA	TER RETROFIT	UPPER BREWSTER HILL ROAD	JOB NO:15-031 DATE: 8/11/16 SCALE: 1" = 150'
E RESULTS	DESIGNED BY: RAR CHECKED BY: RAR		TOWN OF SOUTHEAST	SE-1A
	DRAWN BT: JBM			

SE-1A - Upper Brewster Hill Road: Trapezoidal Channel Stabilization P-Loading Calculation						
Channel ID	A (Private)	B (Private)	C (Private)	D (Private)	E (Private)	F (Private)
Channel Depth - y (ft)	3.0	3.0	3.0	3.0	2.5	1.5
Channel Bottom Width - B (ft)	2.0	2.0	2.0	2.0	2.0	1.0
Channel Top Width -T (ft)	14.0	14.0	14.0	14.0	12.0	7.0
Wetted Perimeter Calculation- P (ft)	15.42	15.42	15.42	15.42	13.18	7.71
Channel Length-L (ft)	209	100	39	57	236	295
Soil Erosion Depth-D (ft)	0.065	0.065	0.065	0.065	0.065	0.065
Soil Erosion Volume-V (ft <sup>3</sup> )	209.4	100.2	39.1	57.1	202.2	147.8
Weight* (lbs)	19,896.0	9,519.6	3,712.7	5,426.2	19,207.7	14,041.5
Weight (Kg)	9,024.8	4,318.1	1,684.1	2,461.3	8,712.6	6,369.2
P Load** (mg/Yr)	2,707,451.8	1,295,431.5	505,218.3	738,396.0	2,613,785.1	1,910,761.5
P Load (Kg/Yr)	2.71	1.30	0.51	0.74	2.61	1.91
				ESTIMATE	D TOTAL (KG/YR):	9.77

#### Notes:

1. Channel dimensions are based upon field measurements estimated by the W&C team during field visits for each channel

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4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

#### Equation and Input Paramaters Basis:

Wetted Perimeter (P) approximately:  $P = T + [(8/3)*(y^2/T)]$ Soil Erosion Volume: V= P\*L\*D BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

Comments:

Private Property referred by the Town of Southeast.





SE-1B - Lower Brewster	SE-TB - Lower Brewster Hill Road. Trapezoidal Channel Stabilization P-Loading Calculation					
Channel ID	A (NYCDEP)	B (Private)	C (Private)	D (Private)	E (Private)	
Channel Depth - y (ft)	3.0	3.0	2.0	2.0	8.0	
Channel Bottom Width - B (ft)	3.0	3.0	1.5	1.5	1.0	
Channel Top Width -T (ft)	15.0	15.0	9.5	9.5	6.0	
Wetted Perimeter Calculation- P (ft)	16.42	16.42	10.44	10.44	17.76	
Channel Length-L (ft)	611	496	200	217	202	
Soil Erosion Depth-D (ft)	0.065	0.065	0.065	0.065	0.065	
Soil Erosion Volume-V (ft <sup>3</sup> )	652.0	529.3	135.8	147.3	233.2	
Weight* (lbs)	61,937.9	50,280.2	12,898.7	13,995.1	22,156.7	
Weight (Kg)	28,095.0	22,807.1	5,850.8	6,348.2	10,050.3	
P Load** (mg/Yr)	8,428,506.1	6,842,126.1	1,755,251.8	1,904,448.2	3,015,090.0	
P Load (Kg/Yr)	8.43	6.84	1.76	1.90	3.02	
			ESTIM	ATED TOTAL (KG/YR):	21.95	

Provider Hill Dood, Transpoidel Channel Stabilization D Loading Coloulation

ESTIMATED TOTAL (KG/YR):

#### Notes:

1. Channel dimensions are based upon field measurements estimated by the W&C team during field visits for each channel

2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

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#### Equation and Input Paramaters Basis:

Wetted Perimeter (P) approximately:  $P = T + [(8/3)*(y^2/T)]$ Soil Erosion Volume: V= P\*L\*D BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

Comments: Public & Private Property referred by the Town of Southeast.

[print page] [close window]









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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-2Prepared for:EOHCPrepared by:REDProject County:Putnam

# "SE-2: Eagles Ridge"

WATER	QUALITY	VOLUME:	WQv(acre-fe	et) = [(P)(R	v)(A)]/12
A = I =	17.7085 a 4.94	acres 27.90%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2 i	nches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.3011		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.3011			
WQv (ac	re-ft) =	0.533			
WQv (cu	I-ft) =	23224			
**Minimu	m Rv = 0.2	when deterr	nining WQv.	Use calcula	ted Rv when determining phosphorus loading.

## **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.3011		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	17.7085		Rv =	Runoff Coefficient	
C =	0.42		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0.67
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0.05
Impervious	0.28
Develped Open Space	0
Weighted "C":	0.42





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>20.69</b> lb/yr
	<b>9.39</b> kg/yr
P Removal>	<b>12.21</b> lb/yr
	<b>5.54</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	17.7 Phosphorus Loading (kg/yr) 9.3		9.39	
Water Quality Volume (cf)	23224	Phosphorus Reduction (kg/yr)	5.54	

### **ASSUMPTIONS/COMMENTS:**

Permission is required from private property owners (assumed to be HOA).

Further investigation should identify location of existing outfalls and potential dry basins. May be able to retrofit old style detention basins.

Potential to utilize adjacent to Town owned Sewage Treatment Facility property.

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-3Prepared for:EOHCPrepared by:REDProject County:Putnam

# "SE-3: Garden Homes Brewster"

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	7.64172	acres	where:	A =	Contributing Area (acres)
=	4.85	63.47%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.6212		WQv =	Water Quality Volume
<b>Rv</b> (min)*	** =	0.6212			
WQv (ac	re-ft) =	0.475			
WQv (cu	-ft) =	20678			
**Minimu	m Rv = 0.2	2 when determ	ining WQv. L	Jse calcula	ted Rv when determining phosphorus loading.

## **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.6212		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	7.64172		Rv =	Runoff Coefficient	
C =	0.44		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0
Commercial	0.36
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.64
Developed Open Space	0
Weighted "C":	0.44



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	<b>19.31</b> lb/yr
	<b>8.76</b> kg/yr
P Removal>	<b>12.94</b> lb/yr
	<b>5.87</b> kg/yr
20% Reduction Due to Site Co	nstraints
P Removal>	10.35 lb/yr
	<b>4.69</b> kg/yr

### Summary:

Proposed Retrofit Practice	Pocket Pond		
Drainage Area (acres)	7.6 Phosphorus Loading (kg/yr) 8.7		
Water Quality Volume (cf)	20678	Phosphorus Reduction (kg/yr)	4.69

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Convert existing retail plaza basin to achieve water quality requirements.

Further study required to determine original practice size and purpose (i.e. conversion of detention facility).

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-4Prepared for:EOHCPrepared by:REDProject County:Putnam

# "SE-4 Number: Lake Tonetta"

A =	1.88084	acres	where:	A =	Contributing Area (acres)
=	1.08	57.42%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.5668		WQv =	Water Quality Volume
<b>Rv</b> (min) <sup>3</sup>	** =	0.5668			
WQv (ac	re-ft) =	0.107			
WQv (cu	-ft) =	4644			
**Minimu	m Rv = 0.3	2 when deterr	nining WQv. L	Jse calcula	ated Rv when determining phosphorus loading.

### **PHOSPHORUS LOADING:**

Simple	e Method:	P Load = P x P j x R v x	C x A x 0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.5668		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.88084		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.57
Developed Open Space	0.43
Weighted "C":	0.41





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Subsurface Infiltration
Removal Efficiency:	100%
P Load>	<b>4.04</b> lb/yr
	<b>1.83</b> kg/yr
P Removal>	<b>4.04</b> lb/yr
	<b>1.83</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Subsurface Infiltration		
Drainage Area (acres)	1.9	Phosphorus Loading (kg/yr)	1.83
Water Quality Volume (cf)	4644	Phosphorus Reduction (kg/yr)	1.83

### **ASSUMPTIONS/COMMENTS:**

Soil tests required to confirm infiltration pratice. Install practice on Town owned property.

8/12/2016

Map Output

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-5Prepared for:EOHCPrepared by:REDProject County:Putnam

# "SE-5: Midtown Trackage Ventures LLC"

WATER	QUALITY	VOLUME:	WQv(acre-fee	t) = [(P)(R)]	/)(A)]/12
A = I =	5.63355 5.01	acres 88.93%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calculated)= 0.8504 Rv (min)**= 0.8504		0.8504 0.8504		WQv =	Water Quality Volume
WQv (ac WQv (cu	re-ft) = -ft) =	0.479 20868			
**Minimu	m Rv = 0.2	2 when detern	nining WQv. L	Jse calcula	ted Rv when determining phosphorus loading.

## **PHOSPHORUS LOADING:**

Simple	Method:	P Load = P x P j x R v x	C x A x 0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.8504		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	5.63355		Rv =	Runoff Coefficient
C =	0.48		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0.11
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.89
Developed Open Space	0
Weighted "C":	0.48





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	<b>59%</b>
P Load>	<b>21.25</b> lb/yr
	<b>9.64</b> kg/yr
P Removal>	<b>12.54</b> lb/yr
	<b>5.69</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	5.6	Phosphorus Loading (kg/yr)	9.64
Water Quality Volume (cf)	20868	Phosphorus Reduction (kg/yr)	5.69

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner. Metro North commuter lot for the Southeast Train Station.

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		<image/>
0 50 100 150 200 Feet	2. SITE TOPOGRAPHY (2012) AND I 3. PROPERTY DATA AND STORM SI PROPERTY DATA AND STORM SI	MPERVIOUS AREA (2013) OBTAINED FROM NYCDEP EWER INFRASTRUCTURE OBTAINED FROM TOWN OF SOUTHEAST
RENNIA ENGINEERING DESIGN, PLLC CML - ENVIRONNENTAL - STRUCTURAL 16 Down Vilage Paus, Subis F. P.D. Box 400, Down Plants, NY 12522 Tel: (840) 877 0555 Fax: (845) 877 0556	Proposed Pipe Propos	sed SRP Location
Woodard & Curran Engineering PA PC 709 Westchester Avenue, Suite L2 White Plains, New York 10604 800.807.4080   www.woodardcurran.com COMMITMENT & INTEGRITY DRIVE RESULTS	STORMWATER     RETROFIT       CONCEPT     PLAN       DESIGNED     BY:     RAR       DRAWN     BY:     JBM	MOUNT KISCO MEDICAL GROUP JUE W: 15-031   DATE: 8/11/16   SCALE: 1" = 100'   TOWN OF SOUTHEAST SE-6



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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-6Prepared for:EOHCPrepared by:REDProject County:Putnam

# "SE-6: Mount Kisco Medical Group"

WATER	QUALITY	VOLUME:	WQv(acre-fe	et) = [(P)(R	v)(A)]/12
A =   =	4.35135 a 2.27	acres 52.17%	where:	A =   =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2 i	nches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.5195		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.5195			
WQv (acre-ft) = 0.226					
WQv (cu-ft) = 9847					
**Minimum Rv = 0.2 when determining WQv.		Use calcula	ted Rv when determining phosphorus loading.		

## **PHOSPHORUS LOADING:**

Simple	Method:	P Load = P x P j x R v x	C x A x 0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.5195		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	4.35135		Rv =	Runoff Coefficient
C =	0.42		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Are	ea
Residential	0	
Commercial	0.48	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.52	
Developed Open Space	0	
Weighted "C":	0.42	





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>8.80</b> lb/yr
	<b>3.99</b> kg/yr
P Removal>	5.19 lb/yr
	<b>2.35</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	4.4	Phosphorus Loading (kg/yr)	3.99
Water Quality Volume (cf)	9847	Phosphorus Reduction (kg/yr)	2.35

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Further soils investigation should identify if infiltration could be a suitable alternative practice. Potential that owner may look to expand site in the future.

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:Powers Products III LLCPrepared for:EOHCPrepared by:REDProject County:Putnam

## "SE-7: Powers Products III LLC"

WATER QUALITY VOLUME:	WQv(acre-feet) = [(P)(Rv)(A)]/12
-----------------------	----------------------------------

A =	11.7481	acres	where:	A =	Contributing Area (acres)
=	3.74	31.83%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.3365		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.3365			
WQv (ac	re-ft) =	0.395			
WQv (cu	I-ft) =	17221			
**Minimu	m Rv = 0.3	2 when deterr	nining WQv. L	Jse calcula	ated Rv when determining phosphorus loading.

### **PHOSPHORUS LOADING:**

Simple	e Method:	P Load = P x P j x R v x	C x A x 0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.3365		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	11.7481		Rv =	Runoff Coefficient
C =	0.38		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Are	ea
Residential	0	
Commercial	0.63	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0.05	
Impervious	0.32	
Developed Open Space	0	
Weighted "C":	0.38	





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>13.87</b> lb/yr
	<b>6.29</b> kg/yr
P Removal>	<b>8.19</b> lb/yr
	<b>3.71</b> kg/yr

### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	11.7Phosphorus Loading (kg/yr)6.29			
Water Quality Volume (cf)	17221	Phosphorus Reduction (kg/yr)	3.71	

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Soils investigation should be completed to identify if infiltration could be a suitable alternative practice. Bioretention could also be utilized and would provide a larger phosphorus reduction.

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-8Prepared for:EOHCPrepared by:REDProject County:Putnam

## "SE-8: Scolpino Park"

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R)]	v)(A)]/12
A = I =	2.96575 1.31	acres 44.17%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.4475		WQv =	Water Quality Volume
<b>Rv</b> (min) <sup>3</sup>	** =	0.4475			
WQv (ac	re-ft) =	0.133			
WQv (cu	-ft) =	5782			
**Minimu	m Rv = 0.2	2 when detern	hining WQv. J	Jse calcula	ted Rv when determining phosphorus loading.

### **PHOSPHORUS LOADING:**

Simple	Method:	P Load = P x Pj x Rv x	C x A x 0.	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.4475		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	2.96575		Rv =	Runoff Coefficient
C =	0.41		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0.56
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.44
Developed Open Space	0
Weighted "C":	0.41



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### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	<b>59%</b>
P Load>	<b>5.01</b> lb/yr
	<b>2.27</b> kg/yr
P Removal>	<b>2.95</b> lb/yr
	<b>1.34</b> kg/yr

### Summary:

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	3.0 Phosphorus Loading (kg/yr) 2.27		
Water Quality Volume (cf)	5782	Phosphorus Reduction (kg/yr)	1.34

### ASSUMPTIONS/COMMENTS:

Install practice on Town owned property.

Soils investigation should be completed to identify if infiltration could be a suitable alternative practice.

Bioretention could also be utilized and would provide a larger phosphorus reduction.

May be potential to treat adjacent ballfield areas.

Adjacent wetland will require a delineation to confirm area available for practice.

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #: SE-9 Prepared for: EOHC Prepared by: RED Project County: Putnam

## "SE-9: 15 Mt. Ebo Road South"

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R)]	v)(A)] /12
A =   =	5.0229 3.19	acres 63.51%	where:	A =   =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2			P = Rv =	Runoff Coefficient [0.05 + 0.009(I)]
RV (calculate $RV$ (min) <sup>3</sup>	ilated)= ** <b>=</b>	0.6216 0.6216		vvQv =	water Quality Volume
WQv (ac	re-ft) =	0.312			
**Minimu	m Rv = 0.2	2 when deteri	mining WQv. l	Jse calcula	ted Rv when determining phosphorus loading.

### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.6216		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	5.0229		Rv =	Runoff Coefficient	
C =	0.44		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0
Commercial	0.37
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.63
Developed Open Space	0
Weighted "C":	0.44





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	<b>59%</b>
P Load>	<b>12.65</b> lb/yr
	<b>5.74</b> kg/yr
P Removal>	<b>7.46</b> lb/yr
	<b>3.39</b> kg/yr

### Summary:

Proposed Retrofit Practice	Surface Sand Filter		
Drainage Area (acres)	5.0 Phosphorus Loading (kg/yr) 5.74		
Water Quality Volume (cf)	13600	Phosphorus Reduction (kg/yr)	3.39

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Bioretention could also be utilized and would provide a larger phosphorus reduction.

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:SE-10Prepared for:EOHCPrepared by:REDProject County:Putnam

## "SE-10: 16 Mt. Ebo Road South"

WATER QUALITY VOLUME:		WQv(acre-feet) = [(P)(Rv)(A)]/12			
A =   = P =	2.81477 1.52	acres 54.00% inches	where:	A =   = P =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in)
Rv (calcu Rv (min) <sup>3</sup>	llated)=	0.5360 0.5360		Rv = WQv =	Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
WQv (ac WQv (cu **Minimu	<b>re-ft) =</b> - <b>ft) =</b> m Rv = 0.2	<b>0.151</b> <b>6572</b> 2 when detern	nining WQv. U	lse calcula	ted Rv when determining phosphorus loading.

## **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.5360		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	2.81477		Rv =	Runoff Coefficient	
C =	0.43		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area	ł
Residential	0	
Commercial	0.46	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.54	
Developed Open Space	0	
Weighted "C":	0.43	





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>5.91</b> lb/yr
	<b>2.68</b> kg/yr
P Removal>	<b>3.49</b> lb/yr
	<b>1.58</b> kg/yr

### Summary:

Proposed Retrofit Practice	Surface Sand	ce Sand Filter		
Drainage Area (acres)	2.8 Phosphorus Loading (kg/yr) 2.6			
Water Quality Volume (cf)	6572	Phosphorus Reduction (kg/yr)	1.58	

### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Soils investigation should be completed to identify if infiltration could be a suitable alternative practice. Bioretention could also be utilized and would provide a larger phosphorus reduction.

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COMMITMENT	& INTEGRITY DRIVE RESULTS

WOODARD

& CURRAN

DESIGNED BY: RAR CHECKED BY: RAR DRAWN BY: JBM TOWN OF SOUTHEAST

SE-11

SE-11 - Highview Terrace: Trapezoidal Channel Stabilization P-Loading Calculation					
Channel ID	A (Putnam County)	B (Private)			
Channel Depth - y (ft)	5.0	4.0			
Channel Bottom Width - B (ft)	1.0	1.0			
Channel Top Width -T (ft)	6.0	5.0			
Wetted Perimeter Calculation- P (ft)	12.18	9.94			
Channel Length-L (ft)	105	80			
Soil Erosion Depth-D (ft)	0.065	0.065			
Soil Erosion Volume-V (ft <sup>3</sup> )	83.1	51.7			
Weight* (lbs)	7,897.4	4,912.5			
Weight (Kg)	3,582.3	2,228.3			
P Load** (mg/Yr)	1,074,682.0	668,489.0			
P Load (Kg/Yr)	1.07	0.67			
EST	IMATED TOTAL (KG/YR):	1.74			

### Notes:

1. Channel dimensions are based upon field measurements estimated by the W&C team during field visits for each channel 2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis:

Wetted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soil Erosion Volume: V= P\*L\*D BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

Comments:

Public & Private Property referred by the Town of Southeast.

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SE-12 - Federal Hill Road: Trapezoidal Channel Stabilization P-Loading Calculation					
Channel ID	A (Private)	B (Private)	C (Private)		
Channel Depth - y (ft)	2.0	3.0	3.0		
Channel Bottom Width - B (ft)	1.5	1.0	2.0		
Channel Top Width -T (ft)	3.0	3.0	4.0		
Wetted Perimeter Calculation- P (ft)	5.77	7.32	8.32		
Channel Length-L (ft)	220	142	100		
Soil Erosion Depth-D (ft)	0.065	0.065	0.065		
Soil Erosion Volume-V (ft <sup>3</sup> )	82.5	67.6	54.1		
Weight* (lbs)	7,841.3	6,422.5	5,140.4		
Weight (Kg)	3,556.8	2,913.3	2,331.7		
P Load** (mg/Yr)	1,067,039.3	873,978.7	699,507.4		
P Load (Kg/Yr)	1.07	0.87	0.70		
	EST	IMATED TOTAL (KG/YR):	2.64		

### Notes:

1. Channel dimensions are based upon field measurements estimated by the W&C team during field visits for each channel 2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Paramaters Basis:

Wetted Perimeter (P) approximately: P= T+ [(8/3)\* (y<sup>2</sup>/T)] Soil Erosion Volume: V= P\*L\*D BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

### Comments:

Private Property referred by the Town of Southeast (former Melrose School Site).

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# PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:PW-1Prepared for:EOHCPrepared by:REDProject County:Dutchess

## "PW-1: 158 Route 22 LLC"

WATER QUALITY VOLUME: WQv(a	acre-feet) = [(P)(Rv)(A)]/12
-----------------------------	------------------------------

A =	5.09019	acres	where:	A =	Contributing Area (acres)
=	4.73	92.92%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	lated)=	0.8863		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.8863			
WQv (ac	re-ft) =	0.451			
WQv (cu	-ft) =	19652			
**Minimu	m Rv = 0.3	2 when detern	nining WQv. L	Jse calcula	ated Rv when determining phosphorus loading.

## **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.8863		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	5.09019		Rv =	Runoff Coefficient	
C =	0.49		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area	
Residential	0	
Commercial	0.07	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.93	
Developed Open Space	0	
Weighted "C":	0.49	





### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond		
Removal Efficiency:	67%		
P Load>	<b>20.27</b> lb/yr		
	<b>9.20</b> kg/yr		
P Removal>	13.58 lb/yr		
	<b>6.16</b> kg/yr		

### Summary:

Proposed Retrofit Practice	Pocket Pond			
Drainage Area (acres)	5.1	Phosphorus Loading (kg/yr)	9.20	
Water Quality Volume (cf)	19652	Phosphorus Reduction (kg/yr)	6.16	

### ASSUMPTIONS/COMMENTS:

Permission required from private property owner.

Calculations include total combined area for 2 Pocket Ponds.

Soils investigation should be completed to identify if infiltration could be a suitable alternative practice. Captures runoff from existing retail center buildings and parking lot.

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- 2.
- 3. 4.
- MAP SOURCE OBTAINED FROM ARCGIS WORLD IMAGERY SITE TOPOGRAPHY (2012) AND IMPERVIOUS AREA (2013) OBTAINED FROM NYCDEP PROPERTY DATA AND STORM SEWER INFRASTRUCTURE OBTAINED FROM TOWN OF PAWLING CHANNEL STABILIZATION PROJECTS PROPOSED WITHIN CLASSIFIED STREAMS REQUIRE CASE BY CASE REVIEW AND APPROVAL BY NYSDEC, AS WELL AS AN APPROVAL OF THE PROPOSED STABILIZATION METHOD.
- STABILIZATION METHOD. THE PHOSPHORUS VALUES INCLUDED IN THIS RETROFIT PLAN ARE ESTIMATED VALUES. FINAL SIGNED AND SEALED PHOSPHORUS LOADING CALCULATION WILL NEED TO BE PERFORMED IN ACCORDANCE WITH THE EOHWC DESIGN MANUAL CONSISTENT WITH THE LATEST APPROVED NYSDEC "ALTERNATIVE CHANNEL STABILIZATION FORMULA". THE FINAL CALCULATION SHOULD INCLUDE SURVEYS TO CONFIRM CHANNEL DIMENSIONS, AND A COMPLETE ANALYSIS AND COMPUTATIONS OF ALL INPUT PARAMETERS USED IN THE "ALTERNATIVE CHANNEL STABILIZATION FORMULA", INCLUDING THE BEHI AND NBS INDEXES. 5.

CML ENVIRONMENTAL • STRUCTURAL   Edword Village Plaza, Suite 5, P.O. Box 400, Doer Flave, NY 12522   Tel: (44) 877-0525 Fac: (84) 877-0526		Channel to be Stabilized	
		Parcels	
	Woodard & Curran Engineering PA PC 709 Westchester Avenue, Suite L2 White Plains, New York 10604 800 807 4090 L www.woodarduuran.com	STORMWATER RETROFIT	DALEY, JOHN 3874 ROUTE 55
	COMMITMENT & INTEGRITY DRIVE RESULTS	DESIGNED BY: RAR CHECKED BY: RAR DRAWN BY: JBM	TOWN OF PAWLING

25

50

75

100

Feet Legend

PW-2

JOB NO:15-03 DATE: SCALE:

PW-2 - Daley John: Parabolic Channel Stabilization P-Loading Calculation				
Channel ID	A (Private)			
Channel Depth - y (ft)	4.0			
Channel Top Width -T (ft)	8.0			
Wetted Perimeter Calculation- P (ft)	13.32			
Channel Length-L (ft)	268			
Soil Erosion Depth-D (ft)	0.065			
Soil Erosion Volume-V (ft <sup>3</sup> )	232.0			
Weight* (lbs)	22,043.3			
Weight (Kg)	9,998.8			
P Load** (mg/Yr)	2,999,647.9			
P Load (Kg/Yr)	3.00			
ESTIMATED TOTAL (KG/YR):	3.00			

ESTIMATED TOTAL (KG/YK):

#### Notes:

1. Channel dimensions are based upon field measurements estimated by the W&C team during field visits for each channel 2. The soil erosion depth has been assumed to be 0.065, and is a conservative assumption based upon the statistical analysis and results included in the study titled "A Practical Method of Computing Streambank Erosion Rate". This study was the basis of the revised approved channel stabilization methodology/calculations as approved by NYSDEC. The assumed 0.065 value was based specifically on the data presented in Figures 2 and 3 titled "Stream Bank Erodibility", that correspond to Low Bank Erosion Hazard Index and Low Near Bank Stress ratings.

3. The phosphorus values included in this retrofit plan are estimated values. Final signed and sealed phosphorus loading calculations will need to be performed in accordance with the EOHWC Design Manual consistent with the latest approved NYSDEC "Alternative Channel Stabilization Formula". The final calculations should include surveys to confirm channel dimensions, and a complete analysis and computations of all input parameters used in the "Alternative Channel Stabilization Formula", including the BEHI and NBS indexes.

4. Channel stabilization projects proposed within classified streams require case by case review and approval by NYSDEC, as well as an approval of the proposed stabilization method.

Equation and Input Parameters Basis: Wetted Perimeter (P) approximately:  $P = T + [(8/3)^* (y^2/T)]$ Soil Erosion Volume: V= P\*L\*D BD\* = bulk density (typ. 95 lb/CF) Ptest\*\* = phosphorus level in soil (typ. 300 mg/kg)

Comments:

Private Residential Property referred by the Town of Pawling.

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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:PW-3Prepared for:EOHCPrepared by:REDProject County:Dutchess

#### "PW-3: Pawling Fire House"

WATER	QUALITY	VOLUME:	WQv(acre-fe	et) = [(P)(	Rv)(A)] /12
A = I = P =	14.5792 1.81 1.2	acres 12.41% inches	where:	A =   = P = By =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in) Runoff Coefficient I0 05 + 0 009(1)]
Rv (calco Rv (min) WQv (ad WQv (cu **Minimu	ulated)= ** <b>=</b> c <b>re-ft) =</b> <b><i>I</i>-ft) =</b> Im Rv = 0.	0.1617 0.2000 <b>0.292</b> <b>12701</b> 2 when dete	rmining WQv.	WQv =	Water Quality Volume

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

0.145 hours	Tc =	Time of Concentration (hours)
84	CN =	Curve Number
526.256	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
2.87714 CFS	Qp =	Peak Discharge (CFS)
	0.145 hours 84 526.256 2.87714 CFS	0.145 hours         Tc =           84         CN =           526.256         qu =           2.87714 CFS         Qp =

#### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x P j x R v x	x C x A x 0.	.103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.1617		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	14.5792		Rv =	Runoff Coefficient
C =	0.47		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total A	rea
Residential	0	
Commercial	0.16	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.84	
Developed Open Space	0	
Weighted "C":	0.47	



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION

Proposed Retrofit Practice:	Proprietary Filtering
Removal Efficiency:	40%
P Load>	<b>10.28</b> lb/yr
	<b>4.66</b> kg/yr
P Removal>	<b>4.11</b> lb/yr
	<b>1.87</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Proprietary Filtering		
Drainage Area (acres)	14.6	Phosphorus Loading (kg/yr)	4.66
Water Quality Volume (cf)	12701	Phosphorus Reduction (kg/yr)	1.87

#### **ASSUMPTIONS/COMMENTS:**

Install practice on property owned by Pawling Fire Dept Inc.

Assumes the installation of curb and storm collection pipe along west side of driveway.

Adjacent wetland will require a delineation to confirm area available for practice.

Further soils and topographic investigation should be completed to identify if surface sand filters could be a suitable alternative practice.

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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:PW-4Prepared for:EOHCPrepared by:REDProject County:Dutchess

#### "PW-4: South Street"

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(R	v)(A)]/12
A =   =	27.3984 2.55	acres 9.31%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
<b>Rv</b> (calculated)= 0.1338		0.1338		WQv =	Water Quality Volume
<b>Rv</b> (min) <sup>3</sup>	** =	0.2000			
WQv (acre-ft) = 0.548					
WQv (cu	-ft) =	23870			
**Minimu	m Rv = 0.2	2 when deterr	nining WQv. l	Jse calcula	ted Rv when determining phosphorus loading.

#### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.1338		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	27.3984		Rv =	Runoff Coefficient	
C =	0.32		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0.1
Commercial	0
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.09
Developed Open Space	0.81
Weighted "C":	0.32





#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Multiple Pond
Removal Efficiency:	76%
P Load>	<b>10.95</b> lb/yr
	<b>4.97</b> kg/yr
P Removal>	8.32 lb/yr
	3.77 kg/yr

#### Summary:

Proposed Retrofit Practice	Multiple Pone	t	
Drainage Area (acres)	27.4	Phosphorus Loading (kg/yr)	4.97
Water Quality Volume (cf)	23870	Phosphorus Reduction (kg/yr)	3.77

#### **ASSUMPTIONS/COMMENTS:**

Install practice on property owned by the Town of Pawling.

Assumes the installation of additional swales or storm collection pipe along South Street. Landscape screening from adjacent neighbor will be required.

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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:VPW-1Prepared for:EOHCPrepared by:REDProject County:Dutchess

#### "VPW-1: Mizzentop Day School"

WATER	QUALITY	VOLUME:	WQv(acre-fee	$e^{t} = [(P)(R)]$	v)(A)]/12
A = I =	3.99598 2.16	acres 54.05%	where:	A = I =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.5365		WQv =	Water Quality Volume
<b>Rv</b> (min) <sup>3</sup>	** =	0.5365			
<i>WQv (acre-ft)</i> = 0.214					
WQv (cu	I-ft) =	9338			
**Minimu	m Rv = 0.2	2 when detern	nining WQv. l	Jse calcula	ted Rv when determining phosphorus loading.

#### **PHOSPHORUS LOADING:**

Simple Method:		P Load = P x Pj x Rv x C x A x 0.103			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.5365		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	3.99598		Rv =	Runoff Coefficient	
C =	0.43		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area	ł
Residential	0	
Commercial	0.46	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.54	
Developed Open Space	0	
Weighted "C":	0.43	



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Pocket Pond
Removal Efficiency:	67%
P Load>	<b>8.40</b> lb/yr
	<b>3.81</b> kg/yr
P Removal>	5.63 lb/yr
	<b>2.55</b> kg/yr

#### Summary:

Proposed Retrofit Practice Pocket Pond			
Drainage Area (acres)	Area (acres)4.0Phosphorus Loading (kg/yr)3.8		
Water Quality Volume (cf)	9338	Phosphorus Reduction (kg/yr)	2.55

#### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner.

Existing site contains a private school and offices.

Adjacent parcel owned by Inspirational Book Service Inc. appears to be part of the drainage area.

8/10/2016

Map Output

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COMMITMENT	& INTEGRITY	DRIVE RESULTS

DESIGNED BY: RAR DRAWN BY: JBM

CHECKED BY: RAR

VILLAGE OF PAWLING



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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	VPW-2
Prepared for:	EOHC
Prepared by:	RED
Project County:	Dutchess

#### "VPW-2: Lappas Inc."

WATER	QUALITY	VOLUME:	WQv(acre-fee	P(P) = [(P)(F)	Rv)(A)] /12
A = I =	3.135 2.46	acres 78.47%	where:	A =   =	Contributing Area (acres) Impervious Area (acres/%)
P =	1.2	inches		P = Rv =	90th Percentile Rainfall Event Number (in) Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcı Rv (min) WQv (ad WQv (cı	ulated)= ** = : <b>re-ft)</b> = <b>ı-ft) =</b>	0.7562 0.7562 <b>0.237</b> 10327		WQv =	Water Quality Volume
**Minimu	ım Rv = 0.	2 when dete	rmining WQv.	Use calcul	ated Rv when determining phosphorus loading.

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

Tc =	0.098 hours	Tc =	<ul> <li>Time of Concentration (hours)</li> </ul>
CN =	97	CN =	<ul> <li>Curve Number</li> </ul>
qu =	610.509	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	2.71381 CFS	Qp =	<ul> <li>Peak Discharge (CFS)</li> </ul>

#### PHOSPHORUS LOADING:

Simple Method:		$P Load = P \times P j \times R \vee X C \times A \times 0.103$			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.7562		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	3.135		Rv =	Runoff Coefficient	
C =	0.47		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Area
Residential	0
Commercial	0.21
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.79
Developed Open Space	0
Weighted "C"	: 0.47



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#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Proprietary Filtering
Removal Efficiency:	40%
P Load>	<b>10.17</b> lb/yr
	<b>4.61</b> kg/yr
P Removal>	<b>4.07</b> lb/yr
	<b>1.84</b> kg/yr

#### Summary:

Proposed Retrofit Practice Proprietary Filtering			
Drainage Area (acres)	3.1 Phosphorus Loading (kg/yr) 4.61		
Water Quality Volume (cf)	10327	Phosphorus Reduction (kg/yr)	1.84

#### ASSUMPTIONS/COMMENTS:

Permission required from private property owner.

One retail building is currently not in use.

Captures runoff from existing retail center buildings and parking lot prior to discharge into the Village of Pawling storm drain system.

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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:VPW-3Prepared for:EOHCPrepared by:REDProject County:Dutchess

#### "VPW-3: Saint Johns Church"

A =	1.55459	acres	where:	A =	Contributing Area (acres)
=	1.05	67.54%		=	Impervious Area (acres/%)
P =	1.2	inches		P =	90th Percentile Rainfall Event Number (in)
				Rv =	Runoff Coefficient [0.05 + 0.009(I)]
Rv (calcu	ulated)=	0.6579		WQv =	Water Quality Volume
<b>Rv</b> (min)	** =	0.6579			
WQv (ac	re-ft) =	0.102			
WQv (cu	I-ft) =	4455			
**Minimu	m Rv = 0.2	2 when detern	nining WQv. L	Jse calcula	ated Rv when determining phosphorus loading.

#### **PHOSPHORUS LOADING:**

Simple	Method:	P Load = P x P j x R v x	C x A x 0.1	103
P =	45	where:	P Load=	Annual load (kg/yr)
Pj =	0.9		P =	Annual Rainfall (inches)
Rv =	0.6579		Pj =	Fraction of rainfall producing Runoff = 0.9
A =	1.55459		Rv =	Runoff Coefficient
C =	0.45		C =	Pollutant Concentration (mg/l)
			A =	A = Contributing Area (acres)

Land Use	% of Total Area
Residential	0
Commercial	0.32
Industrial	0
Actively Grazed Pasture	0
Forest	0
Impervious	0.68
Developed Open Space	0
Weighted "C":	0.45





#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Surface Sand Filter
Removal Efficiency:	59%
P Load>	<b>4.22</b> lb/yr
	<b>1.91</b> kg/yr
P Removal>	<b>2.49</b> lb/yr
	<b>1.13</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Surface Sand Filter			
Drainage Area (acres)	1.6 Phosphorus Loading (kg/yr) 1.9		1.91	
Water Quality Volume (cf)	4455	Phosphorus Reduction (kg/yr)	1.13	

#### **ASSUMPTIONS/COMMENTS:**

Permission required from private property owner. Existing site contains a Church and parking lot. Adjacent parcels contribute to the drainage area. Parcel owned by the Catholic Church Association.

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#### PHOSPHORUS LOADING AND REDUCTION CALCULATION SHEET

Project #:	VPW-4
Prepared for:	EOHC
Prepared by:	RED
Project County:	Dutchess

#### "VPW-4: Fairway Drive"

WATER	QUALITY	VOLUME:	WQv(acre-fee	et) = [(P)(F	Rv)(A)] /12
A = I = P =	20.9297 4.49 1.2	acres 21.45% inches	where:	A =   = P =	Contributing Area (acres) Impervious Area (acres/%) 90th Percentile Rainfall Event Number (in)
Rv (calcu Rv (min) WQv (ac WQv (cu	ulated)= ** = cre-ft) = u-ft) =	0.2431 0.2431 <b>0.509</b> <b>22161</b>		Rv = WQv =	Runoff Coefficient [0.05 + 0.009(I)] Water Quality Volume
winimu	$\operatorname{Im} \operatorname{RV} = 0.$	2 when deter	mining wQv.	Use calcul	ated RV when determining phosphorus loading.

#### WQv PEAK FLOW:

Based upon NYSDEC Stormwater Manual. Appendix B-2

1		11	
Tc =	0.488 hours	Tc =	Time of Concentration (hours)
CN =	86	CN =	Curve Number
qu =	369.334	qu =	Unit Peak Discharge (cfs/mi <sup>2</sup> /inch)
Qp =	3.52309 CFS	Qp =	Peak Discharge (CFS)

#### PHOSPHORUS LOADING:

Simple Method:		$P Load = P \times P j \times R \vee X C \times A \times 0.103$			
P =	45	where:	P Load=	Annual load (kg/yr)	
Pj =	0.9		P =	Annual Rainfall (inches)	
Rv =	0.2431		Pj =	Fraction of rainfall producing Runoff = 0.9	
A =	20.9297		Rv =	Runoff Coefficient	
C =	0.43		C =	Pollutant Concentration (mg/l)	
			A =	A = Contributing Area (acres)	

Land Use	% of Total Are	ea
Residential	0.79	
Commercial	0	
Industrial	0	
Actively Grazed Pasture	0	
Forest	0	
Impervious	0.21	
Developed Open Space	0	
Weighted "C":	0.43	



6 Dover Wilage Plaza, Suite S. P.O. Ben 400, Dover Plaza, KY 12522 Tat. (S46): 677-8565 - Fax: (846): 677-8560



#### PROPOSED RETROFIT PRACTICE AND ANITICIPATED REDUCTION:

Proposed Retrofit Practice:	Proprietary Filtering
Removal Efficiency:	40%
P Load>	20.06 lb/yr
	<b>9.10</b> kg/yr
P Removal>	8.02 lb/yr
	<b>3.64</b> kg/yr

#### Summary:

Proposed Retrofit Practice	Proprietary Filtering		
Drainage Area (acres)	20.9	Phosphorus Loading (kg/yr)	9.10
Water Quality Volume (cf)	22161	Phosphorus Reduction (kg/yr)	3.64

#### **ASSUMPTIONS/COMMENTS:**

Install practice in concrete vault within the Village of Pawling highway Right of Way Drainage area consists mainly of a residential neighborhood.

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## APPENDIX C: STORMBASIN W/ FABPHOS SUBMITTAL & NYSDEC APPROVAL

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From:	Capowski, Robert M (DEC) <robert.capowski@dec.ny.gov></robert.capowski@dec.ny.gov>
Sent:	Tuesday, July 19, 2016 3:41 PM
To:	Steve Lauria
Cn	Kosinski, Kenneth A (DEC)
Subject:	RE: EOHC Years 6-10 - Request to Review Proposed Proprietary Retrofit Practice

Steve,

storm. sized to meet or exceed the peak runoff rate from the contributing subcatchment for the 90% WQV for phosphorus reduction efficiency at 50%. This practice is acceptable for use in EOHWC Stormwater Retrofit Program work and will be credited For filtering practices such as this one, BMPs should be

Thanks, Bob Capowski

# Robert M. Capowski

Environmental Engineer II, Division of Water

New York State Department of Environmental Conservation 625 Broadway Albany, NY 12203 P: (518) 402-8112 | F: (518) 402-9029 | robert.capowski@dec.ny.gov

www.dec.ny.gov | 🚺 | 🖿

Subject: EOHC Years 6-10 - Request to Review Proposed Proprietary Retrofit Practice To: Capowski, Robert M (DEC) <robert.capowski@dec.ny.gov> Sent: Thursday, July 14, 2016 6:42 PM From: Steve Lauria [mailto:slauria@woodardcurran.com]

**TENTION:** This email came from an external sou or click on links from unknown senders or

consideration as an acceptable retrofit practice for use in the East of Hudson Watershed phosphorus reduction program. Good evening Bob, as previosuly discussed please find the attached "Request to Review Proposed Proprietary Retrofit Practice" submittal associated with the FABCO StormBasin (with FABPHOS nutrients filtering cartidge) proprietary practice for your review and

forward to hearing from you. Please feel free to call or email me anytime with any questions. Thank you for your consideration of the attached submittal, and I look

Regards, Steve

COMMITMENT & INTEGRITY	Woodard & Curran Engineering P.A. P.C.	T 800.807.4080
DRIVE RESULTS	709 Westchester Avenue   Suite L2	T 914.448.2266
	White Plains, New York 10604	F 914.448.0147
	www.woodardcurran.com	



July 14, 2016

Mr. Robert M. Capowski, P.E. New York State Department of Environmental Conservation (NYSDEC) New York City Watershed Section Bureau of Water Resource Management, 4<sup>th</sup> Floor 625 Broadway Albany, NY 12233-3505

#### Re: EOHC Stormwater Retrofit Plan, Years 6-10 *Request to Review Proposed Proprietary Retrofit Practice: FABCO StormBasin w/ FABPHOS Nutrients Filtering Cartridge*

Dear Mr. Capowski:

On behalf of the East of Hudson Coalition, we are submitting this "Request to Review Proposed Proprietary Retrofit Practice" submittal for the NYSDEC's review and consideration relative to the East of Hudson Watershed (EOHW) phosphorus reduction program. This submittal represents a request for the NYSDEC to review the proposed proprietary retrofit practice consisting of the FABCO StormBasin w/ FABPHOS Nutrients Filtering Cartridge, for use as an acceptable stormwater retrofit practice in the EOHW phosphorus reduction program.

This submittal includes a description and application of the stormwater treatment practice, field test data documenting phosphorus removal efficiencies, and previously issued regulatory determinations by the Pennsylvania Department of Environmental Protection (PADEP) and Maryland Department of the Environment (MDE) stating that the proposed proprietary stormwater treatment practice qualifies as an acceptable water quality filtering practice in retrofitting and redevelopment applications.

#### **PRODUCT DESCRIPTION & APPLICATION**

The StormBasin is an injection molded basin that is available in custom sizes and can be installed within new drainage structures or used to retrofit existing drainage structures. The proposed product simply is placed within a drainage structure to treat runoff as it enters the structure. An adjustable flange allows the StormBasin to be supported from the interior frame of the drainage structure top casting without interfering with connected inlet and outlet pipes. The StormBasin relies on removable filtration cartridges installed at the base of the basin tub to filter out targeted nutrient pollutants including phosphorus. Stormwater runoff flows vertically through the nutrient filtration cartridge and discharges into the existing drainage structure. Storage within the basin (above the filter) provides capacity for capture and storage of sediment/trash as the pretreatment mechanism prior to treatment via filtration. Bypass ports are provided at the top of the StormBasin to allow for the bypass of heavy rainfall events beyond the design treatment flowrate of the practice. No structural modifications of an existing drainage structure are required for installation of the product. Please refer to the attached manufacturer literature in Attachment A (*page 4 of 38*) for further description and illustrations of the product.

The intended application for this product under the EOHW phosphorus reduction program would be primarily for retrofitting existing drainage structures located in parking lots and roadways that capture runoff from watershed areas comprised of nearly 100% impervious surfaces. Capturing and treating runoff from nearly 100% impervious surfaces would maximize the proposed phosphorus loading, and therefore also maximize the treatment and cost efficiencies of this practice.



The use of this practice would also significantly streamline the stormwater retrofit implementation process. The design and construction phases can be removed from the traditional retrofit implementation process, since the StormBasin retrofit practice simply requires measuring the dimensions of an existing drainage structure and providing them to the manufacturer for production. In addition, the unit can be installed relatively quickly by the owner as it only involves the removal of the existing drainage structure grate, and placing the proposed product within the basin (along with reinstallation of the existing grate). The manufacturer also offers assistance to the Owner during field measurement of existing drainage structures, and installation of proposed units.

The StormBasin is a relatively low cost retrofit option. Depending on the size of the catch basin, the product cost in the range of \$1,000 to \$1,500 per unit. Maintenance of the unit is fairly straightforward and can be performed by the owner; maintenance simply consists of the cleanout of sediment and debris from the StormBasin tub as required, and replacement of the filtering catridge approximately every 3 years (~ \$200 per filter) as recommended by the manufacturer to ensure filtering performance.

#### **REGULATORY APPROVALS**

The StormBasin is recognized by PADEP as a flow based best management practice for water quality treatment under Chapter 6.6 "Runoff Quality/Peak Runoff BMPs" of the *Pennsylvania Stormwater Best Management Practices Manual*, dated December 2006. Based upon correspondence from PADEP staff, the StormBasin product specifically falls under the manual's category of "BMP 6.6.4 Water Quality Filters & Hydrodynamic Devices", and treats phosphorus at a removal rate of 50%. Refer to Attachment B (*page 6 of 38*) which consists of the PADEP correspondence that substantiates this statement, and Attachment C (*page 7 of 38*) for the corresponding excerpt from the Pennsylvania Stormwater Best Management Practices Manual.

In addition to PADEP, the MDE has issued correspondence verifying product classification of the StormBasin for use in retrofitting and redevelopment applications. This verification is can be found in the last paragraph of the MDE letter included in Attachment D (*page 13 of 38*).

#### FIELD TESTING

Fabco Industries Inc. has provided field testing data to document pollutant removal efficiencies, including phosphorus, associated with installations of the catch basin insert product in various sites throughout Long Island. A field testing program was completed that included the study of phosphorus removal at several retrofitted drainage structures within the region. The completed test program analyzed stormwater concentrations of orthophosphate and total phosphate collected from testing sites under existing untreated conditions compared to post treatment via the StormBasin product utilizing the FABPHOS Nutrients Filtering cartridges.

Based upon the provided testing data, average reduction of Total Phosphorus concentration in stormwater runoff was reported at 66% removal for the overall program. A greater average reduction in stormwater orthophosphate concentrations was reported through the testing program at an average of 79% removal. A summary table of the lab testing results is included in Attachment E (*page 14 of 38*), and the field test program report is included in Attachment F (*page 22 of 38*).

#### CONCLUSION

Based on the information noted above, the StormBasin product presents a unique opportunity to introduce a low cost stormwater retrofit practice that would effectively remove high concentrations of phosphorus in runoff from impervious areas into the EOHW phosphorus reduction program. Unlike the currently approved stormwater retrofit practices, the StormBasin is a low cost retrofit solution that is relatively easy and quick to implement (does not require traditional design and construction phases) and maintain, and



does not require any ground intrusive or disruptive construction operations. This product not only has the ability to effectively treat phosphorus, but it also provides the host municipalities with a highly flexible retrofit solution that can be implemented in any existing catch basin within the watershed, regardless of property, ownership, or environmental constraints that have ultimately resulted in cancelled and infeasible stormwater retrofit projects in previous years.

We respectfully request that the StormBasin with FABPHOS Nutrients Filtering Cartridge practice be considered as an acceptable stormwater retrofit practice for implementation within the EOHW phosphorus reduction program, based upon a review of the test data and regulatory agency recognition of the practice included in this submittal. Field verified phosphorus removal rates and outside regulatory agency recognition of the product for water quality treatment support proposed removal rates in the range of 50-65% phosphorus removal.

Thank you for your time and attention towards this matter. Please feel free to contact me directly anytime at <u>slauria@woodardcurran.com</u> or 914-355-9882 with any questions or to discuss this submittal in further detail.

Sincerely,

WOODARD & CURRAN ENGINEERING PA PC

Steven Lauria, PE Associate Principal

Enclosure(s):

Attachment A - FABCO StormBasin filtering catridge product sheets

Attachment B - PADEP correspondence

Attachment C - Pennsylvania Stormwater Best Management Practices Manual excerpt

Attachment D - MDE correspondence

Attachment E - Lab testing summary table

Attachment F - Field testing program report

### **StormBasin**





The StormBasin catch basin insert combines a gross pollutant trap with Fabco's proprietary cartridge filtration system for effective capture of both solid and soluble pollutants. Fabco filter cartridges can be customized with specific media that can target fine particulate, hydrocarbons, heavy metals, organics and other pollutants.

Ideally suited for municipal storm drain retrofits, the StormBasin's solid construction and unique design allow for easy installation and maintenance. The StormBasin also features Fabco's patented dovetailed aluminum flange which enables quick sizing adjustments during installation. Fabco filter cartridges feature a twist and lock mechanism that

makes replacement fast and simple. Periodic maintenance of the StormBasin is quick and easy - trash and debris can be removed from the unit at the street level with a vactor truck or a vacuum hose attached to a sweeper truck. Extracted waste has minimal water content reducing disposal weight and volume.

Fabco's StormPod offers the same filtration method, but for smaller, round openings.

#### **Features/Benefits**

- 1. Easily replaceable lightweight filter cartridges customized for targeted pollutants
- 2. Durable, UV safe co-polymer basin with aluminum mounting flange has a 15 year service life
- 3. Patented dovetailed flange allows for 5" of length/width adjustment during installation
- 4. Baffled bypass traps floatables



Application	Regulatory Issue	Target Pollutants	
Municipal Storm Drain Retrofits	MS4 Permit	Sediment, Trash, O&G, Nutrients	
Fuel/Oil Storage and Handling Facilities	EPA SPCC (Spill Control Rule)	Hydrocarbons, Oily Sediments	
Scrap Metal, Solid Waste, Power Plants	Industrial Multi-Sector General Permit	Solids, Hydrocarbons, Metals	
Pre-Treatment BMP for New Development	Municipal Stormwater Permit	Sediment, O&G, Nutrients	
Retail, Garden Centers Phosphorus, Nitrogen, Pesticides		Fertilizers, Pesticides	


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Part Number	Effectiveness	Ring color code
9718-1	Standard Cartridge Good All-purpose cartridge for common surface runoff that may contain a little bit of everything.	Red
9718-2	Pathogens Cartridge 2x's more pathogen treatment Vs. Std Cartridge. Use near sensitive water ways to keep beaches and shell fishing areas open.	Yellow
9718-3	HV Hydrocarbon Cartridge 25% more hydrocarbon filter media Vs Std cartridge. Excellent for vehicle or maintenance related applications.	Blue
9718-4	HV Metals Cartridge Uses unique FABLITE filter media for HV metals. Suggested for industrial usage where persistent HV metals have been identified in surface runoff	Grey
9718-5	Standard short Cartridge Reduced height version of std Cart.	Mint
9718-6	Nutrients Cartridge Uses proprietary FABPHOS media for nutrients. Highly effective on the critical dissolved Ortho-Phosphates. Helps reduce algae blooms keeping the water clean and healthy.	Green





#### **PADEP** email

From: Rosenquest, Darl [mailto:drosenques@pa.gov] Sent: Friday, August 29, 2014 10:54 AM To: rwoodman@fabcoindustries.com Cc: Himes, William; Lonergan, Mark; Orr, Jennifer Subject: PCSM Approval Request

In response to your submittal, please be advised that the Department does not "approve" proprietary products. It will evaluate the information you submitted to determine whether the BMPs meet or exceed the standards of BMPs contained in the Stormwater manual of 2006. That being said, the initial findings are as follows:

StormBasin and StormSafe Vault essentially fall under the category of Water Quality Filters (BMP 6.6.4). Therefore, no further action is necessary.

DownSpout Filter may have potential for PCSM use, but more information (proper sizing, installation, limitations, etc.) is needed.

Connector Pipe Screen is essentially a trash guard for cross pipes. No further action is necessary.

Trench Drain Filter – It is unclear what the purpose, use, and limitations of this device are. Please provide additional information.

Should a suitable generic design be provided for downspout filters, this BMP will be added to the Department's list of PCSM BMPs. If a purpose and design for the trench drain filter be provided, it too will be added to the list.

Darl Rosenquest, PE, PG | Senior Civil Engineer DEP - Waterways Engineering & Wetlands 25 Technology Drive California Technology Park Coal Center, PA 15423 724-769-1068 drosenques@pa.gov



# **BMP 6.6.4: Water Quality Filters & Hydrodynamic Devices**



A broad spectrum of BMPs have been designed to remove non point source pollutants from runoff as a part of the runoff conveyance system. These structural BMPs vary in size and function, but all utilize some form of settling and filtration to remove particulate pollutants from stormwater runoff, a difficult task given the concentrations and flow rates experienced. Regular maintenance is critical for this BMP. Many water quality filters, catch basin inserts and hydrodynamic devices are commercially available. They are generally configured to remove particulate contaminants, including coarse sediment, oil and grease, litter, and debris.



#### **Other Considerations**

• See Manufacturers specifications for estimated pollutant removal efficiencies.

#### Description

Water Quality Inlets are stormwater inlets that have been fitted with a proprietary product (or the proprietary product replaces the catch basin itself). They are designed to reduce large sediment, suspended solids, oil and grease, and other pollutants, especially pollutants conveyed with sediment transport. They can provide "hotspot" control and reduce sediments loads to infiltration devices. They are commonly used as pretreatment for other BMPs. The manufacturer usually provides the mechanical design, construction, and installation instructions. Selection of the most appropriate device and development of a maintenance plan should be carefully considered by the Designer.

The size of a water quality inlet limits the detention time and the hydraulic capacity influences the effectiveness of the water quality insert. Most products are designed for an overflow in large storm events, which is necessary hydraulically and still allows for a "first flush" treatment.

Regular maintenance according to application and manufacturer's recommendations is essential for continued performance.

#### Variations

#### Tray types

Allows flow to pass through filter media that is contained in a tray located around the perimeter of the inlet. Runoff enters the tray and leaves via weir flow under design conditions. High flows pass over the tray and into the inlet unimpeded.



#### **Bag types**

Insert is made of fabric and is placed in the drain inlet around the perimeter of the grate. Runoff passes through the bag before discharging into the drain outlet pipe. Overflow holes are usually provided to pass larger flows without causing a backwater at the grate. Certain manufactured products include polymers intended to increase pollutant removal effectiveness.



#### Basket types

The insert consists of "basket type" insert that sets into the inlet and has a handle to remove basket for maintenance. Small orifices allow small storm events to weep through, while larger storms overflow the basket. Primarily useful for debris and larger sediment, and requires consistent and frequent maintenance.



#### Simple, "sumps" in inlets

Space created in inlets below the invert of the pipes for sediment and debris to deposit, usually leaving 6-inches to 12-inches at the bottom of an inlet. Small weep holes should be drilled into the bottom of the inlet to prevent standing water for long periods of time. Regular maintenance is required.



#### **Description - Hydrodynamic Devices**

Hydrodynamic Devices are not truly inserts, but separate flow through devices designed to serve in concert with inlets and storm sewer. A variety of products are available from different manufacturers. The primary purpose is to use various methods to remove sediments and pollutants. These methods include baffle plate design, vortex design, tube settler design, inclined plate settler design

or a combination of these. Ideally, the flow through device should remove litter, oil, sediment, heavy metals, dissolved solids and nutrients. Removal ability varies as a result of loading rate and design. Clays and fine silts do not easily settle out unless they are coagulated with some kind of chemical addition or polymer. These devices work most effectively in combination with other BMPs, either as a pre-treatment or as a final treatment at the end of a pipe.



#### **Applications**

Any existing or proposed inlet where the contributing runoff may contain significant levels of sediment and debris, for example: parking lots, gas stations, golf courses, streets, driveways, industrial or commercial facilities, and municipal corporation yards. Commonly used as pretreatment before other stormwater BMPs.

#### **Design Considerations**

- 1. Match site considerations with manufacturer's guidelines/specifications (i.e. land use will determine specific pollutants to be removed from runoff).
- 2. Prevent re-suspension of particles by using small drainage areas and good maintenance.
- 3. Retrofits should be designed to fit existing inlets.
- 4. Placement should be accessible to maintenance.
- 5. If used as part of Erosion & Sedimentation Control during construction, insert should be reconfigured (if necessary) per manufacture's guidelines.
- 6. Overflow should be designed so that storms in excess of the device's hydraulic capacity bypass the treatment and is treated by another quality BMP.

#### **Detailed Stormwater Functions**

### Volume Reduction Calculations

N/A

**Peak Rate Mitigation Calculations** N/A

Water Quality Improvement See manufacturers specifications and tests.

#### **Construction Sequence**

- 1. Stabilize all contributing areas before installing and connecting pipes to these inlets.
- 2. Follow manufacturer's guidelines for installation. Do not use water quality inserts during construction unless product is designed primarily for sediment removal. (Some products have adsorption components that should be installed post-construction.)

#### Maintenance Issues

Follow the manufacturer's guidelines for maintenance, also taking into account expected pollutant load and site conditions. Inlets should be inspected weekly during construction. Post-construction, they should be emptied when over half full of sediment (and trash) and cleaned at least twice a year. They

should also be inspected after runoff events. Maintenance is crucial to the effectiveness of this BMP. The more frequent a water quality insert is cleaned, the more effective it will be. One study (Pitt, 1985) found that WQI's can store sediment up to 60% of its sump volume, and after that, the inflow resuspends the sediments into the stormwater. Some sites have found keeping a log of sediment amount date removed helpful in planning a maintenance schedule. Environmental Technology Verification (ETV) Program and the Technology Acceptance and Reciprocity Partnership (TARP) may be available to assist with the development of a monitoring plan. These programs are detailed in Section 6.3.



Disposal of removed material will depend on the nature of the drainage area and the intent and function of the water quality insert. Material removed from water quality inserts that serve "Hot Spots" such as fueling stations or that receive a large amount of debris should be handling according to DEP regulations for that type of solid waste, such as a landfill that is approved by DEP to accept solid waste. Water quality inserts that primarily catch sediment and detritus from areas such as lawns may reuse the waste on site.

Vactor trucks may be an efficient cleaning mechanism.

Winter Concerns: There is limited data studying cold weather effects on water quality insert effectiveness. Freezing may result in more runoff bypassing the treatment system. Salt stratification may also reduce detention time. Colder temperatures reduce the settling velocity of particles, which can result in fewer particles being "trapped". Salt and sand are significantly increased in the winter, and may warrant more frequent maintenance. Sometimes freezing makes accessing devices for maintenance difficult

#### **Cost Issues**

Check with manufacturers for current prices.

#### **Specifications**

Follow manufacturer's instructions and specific specifications.

#### References

Brzozowski, C., 2003. "Inlet Protection – Strategies for Preserving Water Quality," Stormwater magazine.

Lee, F. "The Right BMPs? Another Look at Water Quality." Stormwater magazine.

- New Hampshire Watershed Management Bureau, Watershed Assistance Section, 2002. "Innovative Stormwater Treatment Technologies BMP Manual."
- Pitt, R. Characterizing and Controling Urban Runoff through Street and Sewerage Cleaning. US EPA, June 1985.

# MARYLAND DEPARTMENT OF THE ENVIRONMENT

1800 Washington Boulevard . Baltimore MD 21230 410-537-3000 • 1-800-633-6101

Martin O'Malley Governor

MDE

Robert M. Summers, Ph.D. Secretary

ATTACHMENT D

Anthony G. Brown Lieutenant Governor

February 13, 2012

Mr. Francis Tighe, Division Manager Eastern Region Fabco Industries, Incorporated 120 Exchange Street, Suite 300 Portland, Maine 04101

Dear Mr. Tighe:

Thank you for your recent email to the Maryland Department of the Environment (MDE), Water Management Administration (WMA) regarding the StormSack, StormBasin and StormSafe Helix products from Fabco Filter Technologies. WMA has evaluated the product descriptions and supporting information with respect to potential treatment applications in Maryland. We offer the following:

In Maryland, environmental site design (ESD) must be used to the maximum extent practicable (MEP) to reduce runoff and mimic natural hydrologic conditions. The use of ESD planning techniques and treatment practices must be exhausted before any approved structural practices may be used. The Fabco products listed above currently do not meet the specifications found in the 2000 Maryland Stormwater Design Manual for ESD or structural practices for new development applications. However, WMA believes that circumstances exist, such as pretreatment, retrofitting, or redevelopment where these practices may be appropriate for water quality treatment.

With respect to the information submitted to support performance claims, please find attached a copy of the fact sheet "Maryland's Stormwater Management Program and Proprietary Practices" that provides additional information on our policies for the review of proprietary practices, including performance monitoring requirements. Monitoring information demonstrating compliance with the general performance criteria must be submitted. MDE recommends that this information conforms to the Technology Acceptance Reciprocity Partnership (TARP) protocol to ensure interstate reciprocity of the data.

WMA has no objections to the use of these Fabco products for redevelopment, pretreatment, and retrofitting provided they are accepted locally. However, local jurisdictions may request that a letter from MDE/WMA be provided verifying product classification. Please consider this that letter. Thank you again for your interest. If you have any additional questions, please contact me at 410-537-3550 or scomstock@mde.state.md.us.

Sincerely,

2 Cemses

Stewart R. Comstock, P.E. Regulatory & Compliance Engineer Sediment, Stormwater & Dam Safety Program

www.mde.state.md.us

# ATTACHMENT E

2	007: Te	esting wit	h Nuti	rients ca	rtridge	FPAM at Cour	ntry La	ake Court, Centerpo	rt, NY		
Cartridge type: FPAM											
Untreated	ID	Report Date						Treated	ID		
Huntington Town, Country Lake Court	0367 (IN)	11/16/07	Value	Sampled	Water LRL	Method		Huntington Town, Country Lake Court	0368 (OUT)	Value	% Change
Tot. Kjeldahl N.	mg/L		3.80	11/12/07	0.2	SM4500NorgB		Tot. Kjeldahl N.	mg/L	2.40	36.84%
Nitrate as N	mg/L		1.40	11/7/07	0.5	EPA353.2		Nitrate as N	mg/L	0.49	65.00%
Nitrogen, total as N	mg/L		5.20	11/12/07	0.2	EPA351,353		Nitrogen, total as N	mg/L	2.90	44.23%
Ortho Phosphate as P	mg/L		0.58	11/7/07	0.1	EPA365.3		Ortho Phosphate as P	mg/L	0.17	70.69%
Tot. Phosphate as P	mg/L		0.57	11/14/07	0.02	EPA365.3		Tot. Phosphate as P	mg/L	0.34	40.35%
Cartridge type: FPAM Untreated	ID	Report						Treated	ID		
Huntington Town,	0365 (INI)	11/9/07	Value	Sampled	Water	Method		Huntington Town,	0366	Value	% Change
Tot Kieldahl N	ma/l		0.80	11/1/07		SM4500NorgB		Tot Kieldahl N	(001) mg/l	0.60	25.00%
Nitrate as N	mg/L		0.00	10/30/07	0.2	EPA353.2		Nitrate as N	mg/L	0.00	0.00%
Nitrogen total as N	mg/L		0.40	11/1/07	0.0	EPA351 353		Nitrogen total as N	mg/L	0.40	25.00%
Ortho Phosphate as P	mg/L		0.00	10/31/07	0.1	EPA365 3		Ortho Phosphate as P	mg/L	0.09	81.63%
Tot. Phosphate as P	mg/L		0.33	11/2/07	0.02	EPA365.3		Tot. Phosphate as P	mg/L	0.09	72.73%
Cartridge type: FPAM											
Untreated	ID	Report Date						Treated	ID		
Huntington Town, Country Lake Court	112101 (IN)	12/4/07	Value	Sampled	Water LRL	Method		Huntington Town, Country Lake Court	112102 (OUT)	Value	% Change
Tot. Kjeldahl N.	mg/L		3.00	11/27/07	0.2	SM4500NORGB		Tot. Kjeldahl N.	mg/L	1.00	66.67%
Nitrate as N	mg/L		1.00	11/27/07	0.5	EPA353.2		Nitrate as N	mg/L	0.50	50.00%
Nitrogen, total as N	mg/L		4.00	11/27/07	0.2	EPA351,353		Nitrogen, total as N	mg/L	1.50	62.50%
Ortho Phosphate as P	mg/L		1.90	11/21/07	0.1	EPA365.3		Ortho Phosphate as P	mg/L	0.26	86.32%
Tot. Phosphate as P	mg/L		2.10	11/30/07	0.1	EPA365.3		Tot. Phosphate as P	mg/L	0.30	85.71%

Avg					
Tot. Kjeldahl N. n	ng/l <b>2.53</b>	Tot. Kjeldahl N.	mg/L	1.33	
Nitrate as N	0.96	Nitrate as N	mg/L	0.49	
Nitrogen, total as N	3.33	Nitrogen, total as N	mg/L	1.67	
Ortho Phosphate as P	0.99	Ortho Phosphate as P	mg/L	0.17	
Tot. Phosphate as P	1.00	Tot. Phosphate as P	mg/L	0.24	
		Avg			
		Tot. Kjeldahl N.			42.84%
		Nitrate as N			38.33%
		Nitrogen, total as N			43.91%
		Ortho Phosphate as P			79.55%
		Tot. Phosphate as P			66.26%

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377 SHEFFIEL	DAVE. • N. BABYLON, N	I.Y. 11703 - (631) 422-6777 - FAX (631) 422-5770
Email: LAB NO.274758.	ecotestiab@aoi.com 01	Website: www.ecotestlabs.com 11/09/07
ATTN ;	Fabco Industries 350 Jerícho Turr Jericho, NY 117 Len Enma	a, Inc. Apika, Suite 300 753-1317 PO#:
SOURCE OF SAMPLE: Source of sample:	Huptington Town,	. Country Lakes Court
COLLECTED BY;	Client DAT TIM	FE COL'D:10/30/07 RECEIVED:10/30/07 E COL'D:1530
MATRIX:Water SA	MPLE: 0365 (IN)	

				DATE OF		ANALYTICAL
ANALYTICAL PARAMETERS	UNITS	RESULT	FLAG	ANALYSIS	LRL	METHOD
Tot. Kjeldahi N.	mg/L	0.0		11/01/07	0.2	SN4500Norg8
Nitrate as N	mg/L	< 0.5		10/30/07	0.5	EPA353.2
Nitrogen, total as N	ag/L	8.0		11/01/07	0.2	SM4500NH3C
ortho Phosphate as P	mg/L	< 0.5	*	10/31/07	0.02	EPA365.3
Tot. Phosphate as P	mg/L	0.33		11/02/07	0.1	EPA365.3

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LRL=Laboratory Reporting Limit

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REMARKS: \*elevated lab reporting limit due to interferenc in sample.

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LAB	Email: ecotestlab@aol.com N0.274758.02	Website: www.ecotestlabs.com 11/09/07

ATTN:	Fabco Industries, Inc. 350 Jericho Turnpike. Sui Jericho, NY 11753-1317 Len Emma	te 300 P0#:	
SOURCE OF SAMPLE:	Huntington Town, Country	L <b>akes Cour</b> t	
SOURCE OF SAMPLE:			
COLLECTED BY;	Client DATE COL'D:1	0/30/07 RECEIVED:10/3	0/0/
	TIME COL'D:15	530	
MATRIX:Water SAM	IPLE: 0366 (OUT)		
		B.( 20 AT	
MAIRIX: WATER SAF	FLC. 0300 (001)	54TC 07	4 VAL VITO 44

			DATE OF		ANALLI I LOAD
ANALYTICAL PARAMETERS	UNITS	RESULT	FLAG ANALYSIS	LRL	METHOD
Tot. Kjeldahl N. 1	og∕L	0.6	11/01/07	0.2	SM4500NorgB
Nitrate as N	ng/l	< 0.5	10/30/07	0.5	EPA353.2
Nitrogen, total as N t	og/L	0,6	11/01/0/	0.2	SM4 500NH3C
ortho Phosphate as P	ng/L	< 0.1	10/31/07	0.1	EPA365.3
Tot. Phosphate as P	ag/1.	< 0.1	11/02/07	0.1	EPA365.3

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#### LRL=Laboratory Reporting Limit

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Email: ecotestlab@aol.com Website: www.ecotestlabs.com LAB\_N0.274866.01 11/16/07

ልተዋል -	Fabco Industries 350 Jericho Turn Jericho, NY 117 Leo Emme	, Inc. pike, Suite 300 53-1317	P0#•	
AIIA,	ach cana		ruw,	
SOUNCE OF SAMPLE: Source of sample:	Huntlagton Town,	Country Lakes	Court	
COLLECTED BY:	Client DATE	COL: D-11/07/07	RECEIVED-11/0	7/07
	TIME	COL D 1300		
MATRIX:Weter SA	MPLE: 0367 (IN)			
			DATE DE	AND STOR

ANALYTTCAL PARAMETERS	INTTS	DESIII T	E1 4 C	ANALVETS	1 21	METHON
Tot Kieldebl N		3 0	r 1.,613	11/19/07	A 3	CHICANNA
Vitesto se N		1.6		11/12/07	0.2	SM4SUUNUEBD
Niture as n	ша/ с	1.4		11/0//0/	0.5	EPA353.2
ALLFOGER, LOLAL AS N	mg/L	5.2		11/12/07	0.2	EPA351,353
ortho Phosphate as P	mg/L	0.58		11/07/07	0.1	EPA365.3
Tot. Phosphale as P	mg/L	0.57		11/14/07	0.02	EPA365.3

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377 SHEFFIELD AVE. + N. BABYLON, N.Y. 11703 - (631) 422-5777- FAX (631) 422-5770

Email: ecotestlab@aol.com Website: www.ecotestlabs.com 1.AB\_N0.274866.02 11/16/07

ATTN;	Fabco Industries, Inc. 350 Jericho Turnpike, S Jericho, NY 11753-1317 Len Emma	uite 300 PO#:	
SOURCE OF SAMPLE:	Huntington Town, Countr	y Lakes Court	
COLLECTED BY:	Client DATE COL'D: TIME COL'D:	11/07/07 RECEIVED:11/07	/07
MATRIX;Water SA	MPLE: 0368 (OUT)	1.700	
		DATE OF	AWALYTICAL

ANALYTICAL PARAMETERS	UNITS	RESULT	FLAG ANALYSIS	LRL	METHOD
Tot. Kjeldahl N.	mg∕L	2.4	11/12/07	0.2	SM4500NorgB
Nitrate as N	mg/L	< 0.5	11/07/07	0.5	EPA353.2
Nitrogen, total as N	mg/L	2.9	11/12/07	<b>D</b> .2	EPA351,353
ortho Phosphale as P	±8/L	0.17	11/07/07	0.02	EPA365.3
Tot. Phosphate as P	wg/l	0.34	11/14/07	0.02	EPA365.3

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LRL=Laboratory Reporting Limit

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# COLEST LABORATORIES, INC.

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Email: ec LAB_NO.275079.0	otestiab@aoi.co 01	m Website: www.ecot 12	estlabs.com 2/04/07
A <b>J</b> "T N :	Fabeo Rodust 350 Jecisbo Jericho, NY Leo Emma	ries, Inc. Turnpike, Snite 300   t1753-1317	PD# :
SOURCE OF SAMPLE; SOURCE OF SAMPLE;	Country Lake	- Dourt	
COLLECTED BY:	Client	DATE COL1D:11/20/07 THE COL1D:1330	RECEIVED:31/21/07
MATRIX;Water SA	MPI.E: 112101		

				DATE OF		ANALYTICAL
ANALYTICAL PARAMETERS	UNITS	RESULT	FLAG	ANALYSIS	1.R1	METHOD
Tot. Kjoldahl N.	mg/L	3.0		31/27/07 (	0.2	SM4500NORGB
Nitrate as N	mg/f	1		11/27/07 0	n.5	EPA353.2
Nitrogen, total as N	mg/1.	4.0		11/27/07 0	0.2	PPA351.353
ortho Phosphate as P	mg∕l.	1.9		11/21/07 0	0.1	EPA365.3
‴ot. ⊅hosphate as P	mg/L_	2.1		11/30/07 (	D.1	EPA365.3

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# ECOTEST LABORATORIES, INC.

ENVIRONMENTAL TESTING

#### 377 SHEFFIELD AVE. • N. BABYLON, N.Y. 11703 • (631) 422-5777• FAX (631) 422-5770

Email: cc 1.AB NO.275079.	otestiab@aoi.co 02	om Website	: www.ecc t	testiabs.com 2/04/07	
ATTEN :	Faboo Indust 350 Jericho Jericho, MY Leo Eome	tries, Inc. Turnpike, 11753-131	Suite 300 2	) P(1#;	
SOURCE OF SAMPLE: SOURCE OF SAMPLE:	Country Cake	e Court			
COLLECTED BY:	Client	DATE COLID TIME COLID	:11/20/07 :1330	RECEIVED:11/2	1707
MATRIX:Water SA	MPLE: 112102				
ANALYTICAL PARAMETERS	UNITS	RCSIO,T	FLAG	DATE OF ANALYSIS LRI	AKALYTTICAL METHOD 2004500000000

Tot. Kjeldahl N.	mg/1.	1	11/27/07	0.2	SM4500NORGB
Nitrate as N	ing∕€.	0.5	11/2//07	0.5	ЕРАЭБЭ.2
Nitrogen, total as N	mg/L	1.5	11/27/07	0.2	EPA351,353
ortho Phosphate as P	mg/L	0.26	11/21/07	0.02	EPA365.3
Tot. Phosphate as P	mg/L	0.3	11/30/07	0.1	EPA365.3

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### <u>FABCO INDUSTRIES, INC</u> <u>STORMWATER NUTRIENTS: P & N</u> <u>TEST PROGRAM</u>



#### **Executive Summary**

Under a contract between a local municipality and Fabco Industries, Inc, Bohemia, NY, from October 2006 to December 2007 a series of field tests were conducted on the Fabco StormBasin and StormPod catch basin inserts to evaluate their effectiveness in reducing phosphorus and nitrogen compounds in stormwater runoff. The testing took place at 3 different sites and involved 5 different filter cartridge configurations.

The testing protocol called for testing under realistic field conditions; all test units were installed into existing roadside storm drains, only minimal maintenance was performed during a test sequence and the same filtering cartridge was used from start to finish better simulating expected results. All samples of treated and untreated stormwater were collected during the first 15 minutes – "first flush" of a rain event. Many published studies (example: First Flush Phenomenon, CalTrans, Aug 2005) have concluded that first flush runoff water contains the highest expected concentrations of pollutants during a storm event.

The data presented in the report confirms that the Fabco StormBasin and StormPod units were highly effective in reducing both phosphorus and nitrogen compounds. Specifically:

- Total phosphates were reduced an average 66% exceeding the 40% required by many states including: New York, Maryland, Virginia and New Jersey.
- Total nitrogen compounds were reduced an average 44%

Additionally, although not required by the study, the report contains information on the type and quantity of solid debris; sediments, trash, leaves, sticks and other material that were collected in the units between tests. Using a separate laboratory analysis on this type

of debris, the report concludes significant concentrations of nutrients maybe stored in this captured material that is not included in the reported reductions.

### <u>FABCO INDUSTRIES, INC</u> <u>STORMWATER NUTRIENTS: P & N</u> <u>TEST PROGRAM</u>

#### Introduction:

At the request of a local municipality, a stormwater monitoring program was initiated by Fabco Industries, Bohemia NY, to investigate the efficacy of using the Fabco StormBasin to reduce the levels of nitrogen and phosphate nutrients in stormwater runoff. These chemical species, which typically result from agricultural/landscaping activities, can give rise to eutrophication and subsequent growth of aquatic plant life in receiving waters. This growth tends to deplete vital dissolved oxygen reserves and can result in fish kills.

Although both nutrient types are important to plant growth many state stormwater programs require stormwater Best Management Practices (BMPs) to reduce only phosphate levels by a specific amount. For example New York State requires a 40% reduction of Total Phosphates. Specific reductions also come into play within the EPA's TMDL program (Total Maximum Daily Load).

#### **Background:**

The Fabco Industries StormBasin is a water treatment system that installs below the iron grate of an existing roadside or parking lot stormwater sewer drain. The StormBasin can be installed into most existing storm water drains without construction or other modifications. In this position the StormBasin intercepts and treats pollutants suspended and/or contained in surface water runoff including: sediments, trash and debris, oils, grease and other toxic hydrocarbon-based chemicals as well as potentially harmful bacteria.

#### The Technology:

The Fabco StormBasin system consists of a large, injection-molded basin for the collection of raw water, sediments and debris and one or more filtering cartridges located at the bottom of the tub, which treat and discharge the clean water into the storm water system. (Appendix A: StormBasin brochure)

The StormBasin cartridges are selected based on actual pollutant loads expected and are user replaceable.



Currently there are five standard

cartridge configurations to choose from: General purpose, Heavy-hydrocarbons (oils & grease), Bacteria, Metals, and Nutrients. Each cartridge type applies one or more filtering technologies in varying degrees to treat specific pollutants. (Appendix B: Filter cartridge brochure)

At the start of the project, Fabco's original nutrient cartridge, although effective on both nitrogen and phosphorous compounds, would not consistently meet the 40%

phosphorous reduction required by many states, including New York. To improve performance on these nutrient compounds Fabco evaluated the use of ten different commercially available filter media in various combinations. Using a series of preliminary, bench scale experiments five were selected for testing within this program.

The media used in this study are identified as:

CHZ – A granular, highly active zeolite mineral which has proven abilities as an ion exchange media.

IC – A fine granular, iron based material specifically produced for efficient removal of phosphates, arsenic and silicates from fresh and salt water. Developed in Germany for treating main water supplies

NP – A filter material that has found wide acceptance in large scale commercial aquariums over the past 20 years. NP is effective on ammonia, heavy metals, phosphates and toxic organics.

FP – Fabco's proprietary FabPhos product that combines the effectiveness and many of the properties of the "IC" and "NP" products.

FPAM – Fabco's antimicrobial treatment applied to FabPhos filter media. The antimicrobial surface reduces bacterial build up and slimes.

Using these materials Fabco assembled and tested 4 types of cartridges, which were designated

- 1. ICCHZ = Combination of layers of IC and CHZ
- 2. NP = Nutrient Pad material used as sole media type
- 3. FPCHZ = Combination of layers of FabPhos and CHZ
- 4. FPAM = Single layer of unique FabPhos material with an additional antimicrobial treatment.

Fabco StormBasin sectional view.	Fabco filtering cartridge. Volume above red ring is considered a "Pre-Filter"

# Locations:

The sites selected for StormBasin installation were chosen from a list of approximately 15 locations provided by the municipality.

Under the terms of the contract Fabco Industries provided and installed 10 StormBasin units during the spring of 2005 in preparation for the testing. Fabco selected 3 sites for nutrients testing:

#### Site descriptions:

#### Site1 community Beach: Base line Nutrient values

The test drain was located in the Northeast corner of the beach parking field and serviced approximately 5900 square feet of black top paving. The parking field was slightly sloped towards the drain causing considerable accumulations of sediments, trash and debris to flow towards the drain. Most importantly for the bacteria study, the parking lot attracts numerous seagulls that leave behind unmistakable evidence of their visits.

Each sewer drain selected at this site had a 24"x48" grate and featured a rear open box inset into the concrete curb. Depth of the vault below the grate was approximately 40".

Fabco Industries installed a 22"x 44" StormBasins (p/n 9731- 1E) which was configured for the rear open curb box. This configuration features a formed rubber flap that extends from the back edge of the tub into the rear open box. This flap enhances the unit's ability to capture the very low flows that are generated during the first flush period of a storm. The StormBasin selected featured two (2) Bacteria filtering cartridges p/n 9718-2 (Yellow ring).

As the waterway adjacent to the beach is federally classified as an impacted waterway (303d) due to pathogens/bacteria pollution this was considered an ideal site for Fabco's bacteria study. The final bacteria report provided by Fabco Industries was completed in December 2006 and is available on the Fabco Industries website (www.fabco-industries.com).

During the bacteria testing phase Fabco engineers had two sets of water samples analyzed for nutrients. It is important to remember that the cartridges used at the beach were optimized for bacteria treatment and as such had no nutrient treatment media in the filter cartridge. The purpose of this sampling was to identify and measure the baseline nutrient values at that site. With virtually no surrounding lawns or landscaped yards in the vicinity, low nutrient levels were expected

#### Site 2 community beach:

The drains at this site were located at the bottom of a steeply sloped driveway entering a popular beach front park. The driveway is narrow, heavily shaded, and does not attract any seagulls. Runoff entering the drains flows very quickly and contains considerable sediment loads. The drains empty directly into the harbor located approximately 400 feet away.

The two (2) storm drains selected had the same configuration and size as the drains at Site 1. However the two grates were situated next to each other and shared a common underground vault.

Fabco Industries installed two (2) 22"x 44" StormBasins (p/n 9731-1E) which were configured similarly to the units at Site 1 except for the cartridges.

As this site was similar to many other sites located along the north shore of Long Island New York it was considered a good site for nutrient testing.

#### Site 3: Residential neighborhood adjacent to waterway

A relatively short dead-end road was selected for the test as it had four well-landscaped properties running parallel to the road surface and the installed storm drains empty into a nearby pond located at the end of the road. Based on direct observations, it is suspected that the vegetation on these properties receives a considerable amount of fertilizer. Inasmuch as the storm drains on this road are routed to an estuarial body of water that ultimately drains to Long Island Sound, the impacts associated with the discharge of nutrients in stormwater are potentially significant.

The drain selected for testing was a 24" round grated inlet very similar to the ones you would see in commercial parking lots. This drain had sufficient depth for the unit and the testing apparatus.

Fabco installed a Round StormPod unit, p/n 9734-1A, which would accept a single Nutrients cartridge.

### **Methods**

The sampling protocol called for the simultaneous collection of both an untreated and treated sample during a rain event. The samples collected were then transported to an independent laboratory<sup>1</sup> for analysis of the following analytes:

3 nitrogen compounds

- Total Kjeldahl or organic nitrogen: animal or human waste, decaying organic matter
- Nitrates (NO<sub>3</sub>): inorganic nitrogen from two (2) sources breakdown of nitrites (NO<sub>2</sub>) by nitrifying bacteria and chemical fertilizers
- Total Nitrogen: representing the sum of inorganic and organic nitrogen

Two types of phosphates

- Total phosphates: Combined organic and inorganic phosphates
- Ortho-phosphates: inorganic, soluble phosphates

Explanation of phosphate analytes:

Phosphorous is usually present in water in the form of phosphates. Phosphates can be organic or inorganic. Organic phosphate is phosphate that is bound to plant tissue, waste solids or other organic material. Inorganic phosphate is not bound to organic material. It can exist as free ions available for immediate plant uptake or attached to sediments. However, plants can only use inorganic free ions also called Ortho-phosphates directly. Organic phosphates must be decomposed into inorganic phosphate before plants can use it for growth.

The monitoring would take place over an indefinite time period with little or no maintenance being performed on the unit during the monitoring period. All samples represent a first flush capture.

#### Automatic sampling at sites 1 & 2

Water samples at sites 1 and 2 were collected automatically using a battery powered, Global Water, Model SS201 Storm water sampler (Appendix C).

The Global unit features a large, watertight plastic case and dual individually controlled peristaltic sampling pumps with 2 sample bottles. For this test, the standard 1-gallon sampling bottles were replaced with smaller 1 liter bottles.

To collect the effluent samples special collection "pails" or "buckets" were designed to attach and seal directly to the bottom of the standard Fabco Cartridge body.



<sup>1</sup> Ecotest Laboratories, Inc, 377 Sheffield Ave, N. Babylon, NY 11703, Tel: 631/422-5777

In the pictures on the right, the standard cartridge body is dark blue. The collection pail area is a light green color and is sealed to the cartridge body with a sealing adhesive.

#### Collection pail features:

Each collection pail was constructed with the following features:

- A vertical over-flow pipe To maintain approximately 2 liters of water in the pail while allowing excess water to escape.
- 2) A quick connect coupling Connects pail to the supply line of the peristaltic pump and sample bottle.
- 3) A sensor switch Activates pumps when the minimum level of water has accumulated in the pail.

Two collection pails were fabricated. The first was attached to the standard Fabco filtering cartridge under test. The second was attached to an empty cartridge body. These two filters were then installed into the bottom of the StormBasin unit with the supply lines routed to the Global Sampler.

#### Sample collection:

During a storm event surface water enters the

StormBasin, flows into and through the cartridges and collects in the pails. When approximately two liters of water has collected, the sensor switch activates the pumps and two **First Flush** water samples are collected. The cartridge with the media left in place would supply a sample of treated water. The empty cartridge would collect a sample of untreated raw water.

#### Semi-Automatic Testing /Sampling at Site 3

The sampling program was set-up to simultaneously collect both the untreated and treated streams of stormwater flowing through the unit. The equipment used was the NALGENE (I-CHEM) Storm Water Sampler (Appendix D). The use of this device permits the remote collection of a sample from the first flush of a qualifying event.

The Nalgene sampler assembly consists of a round black mounting tube and a translucent one liter, plastic sampling bottle that is inserted down into the mounting tube.

Two samplers were used per unit; one was attached to the plastic collection tub and a second was attached to the bottom of the cartridge.

Prior to attaching the mounting tubes, a small hole (3"dia) was drilled in the bottom of the StormPod tub to allow water to pass out and into the sample bottle. This sampler would collect raw untreated water entering the StormPod

To prepare the cartridge a piece of round plastic material with a four inch diameter hole in the center was glued to the bottom of the filter cartridge. This flat plastic washer-like





device insured that water leaving the cartridge would be directed out of a central hole into the mounting tube and to the sample bottles.

The black Nalgene tubes were mounted vertically (extending downwards) from the bottom of the StormPod basin and filter cartridge using clevis pins so that they could be removed when required.

After completing these preparatory steps the white sample bottles were then inserted into the mounting tubes and the assembly was fixed, using the clevis pins, to the StormPod basin and cartridge body. In this configuration the bottle under the Basin would collect the sample of untreated water whereas the bottle under the cartridge would catch a sample of treated water.



#### Sediment Analysis:

As part of the contract, Fabco provided maintenance between testing cycles on the StormBasins to remove collected sediments and debris.

Numerous studies including the National Urban Runoff Program (NURP), which was used as the basis for the NPDES amendments to the Clean Water Act, sight the variety of pollutants, including nutrients that are attached to sediments in runoff.

As part of this study Fabco will include data from one of the maintenance visits.

Additionally, although we did not request a lab analysis of this particular collected waste, we will provide an analysis of a similar waste collected at a Fabco StormBasin site located along the water in Bayville, NY (Appendix E)

# Field testing

Testing/sample collections took place during 5 time periods spanning 2006 and 2007.

Test	Site	Cartridge	Start Date	End Date	# Samples
1	Site 1 (2006)	Bacteria	10/2/06	10/17/06	2
2	Site 3 – Test 1 (2006)	ICCHZ	9/18/06	10/20/06	3
3	Site 3 – Test 2 (2006)	NP	11/16/06	12/19/06	2
4	Site 2 (2007)	FPCHZ	7/06/07	8/02/07	3
5	Site 3 (2007)	FP-AM	11/01/07	11/27/07	3

Table 1: Stormwater sampling

This section provides a brief discussion of the testing that took place during each of the 5 tests. For a quick overview, see individual appendices for each location/Test.

#### 1. <u>Site 1:</u>

Testing was performed at this site in October of 2006. As expected the bacteria cartridges installed in the unit during the test were ineffective on these chemicals. Again the purpose of the test was to obtain a baseline for the runoff concentrations at the site.

Analysis of the raw samples verified that the runoff contained both Phosphorous and Nitrogen compounds in excess of the National median concentrations. The site recorded the highest levels of organic nitrogen (Kjeldahl) in the test. This is probably attributable to the large number of mostly seagulls that inhabit the site. (See appendix F for data)

#### 2. <u>Site 3 (2006): Test 1</u>

Testing was performed during October of 2006. Analysis of the raw samples verified that the runoff contained both Phosphorous and Nitrogen compounds in excess of the National median concentrations.

The cartridge being used for test 1 was a combination of a commercially available Iron rich compound (IC) normally used for Phosphorous control and a zeolite compound (CHZ), which had shown an affinity for nitrogen compounds during in-house testing. Both filtering compounds were granular particles. (Cartridge designated ICCHZ)

Analysis of the results shows good performance on both phosphorus compounds with Total phosphorous being reduced an average 63% and Ortho phosphates being reduced by 69%.

Performance on nitrogen compounds was lower than expected due to poor results obtained in sample set #2.

Sample set 2		Untreated	Treated	% Change
Tot. Kjeldahl N.	mg/L	11.00	19.0	-72.73
Nitrate as N	mg/L	0.49	0.49	0.00
Nitrogen, total as N	mg/L	11.00	19.0	-72.73

Based on an analysis of the filtering cartridge, the poor results were probably related to the CHZ compound.

If we disregard this data point, nitrogen compounds were reduced by the ICCHZ cartridge as follows:

Tot. Kjeldahl reduced an average 36.63% Nitrate reduced an average 29.2% Nitrogen reduced an average 38%

#### Review of test 2:

The IC compound applied in the cartridge consistently reduced phosphorus compounds by greater than 40%. This supports traditional claims regarding the use of Fe compounds in waste water applications and large aquariums.

Results on the nitrogen compounds although encouraging were erratic. Additional testing on the CHZ filter compound is required to confirm effectiveness. (Appendix G for data)

#### 3. <u>Site 3 (2006): Test 2</u>

The second set of tests performed at Site 3 was completed in November-December of 2006. For this test a commercially available filter pad called a Nutrient Pad (NP) was tested in the Fabco filter. The NP pad is a woven, mat-type product made up of bonded thin filaments that have been treated with a proprietary technology. (Cartridge designated NP)

This filter media performed very well in the first sampling for all compounds

First sampling	0330 (OUT)	Value	% reduction
Tot. Kjeldahl N.	mg/L	3.00	25.00%
Nitrate as N	mg/L	0.49	59.17%
Nitrogen, total as N	mg/L	3.00	42.31%
Ortho Phosphate as P	mg/L	0.02	96.36%
Tot. Phosphate as P	mg/L	0.15	72.73%

However, there was a decrease in performance during the second sampling set

Second sampling	0338 (OUT)	Value	% reduction
Tot. Kjeldahl N.	mg/L	9.20	8.00%
Nitrate as N	mg/L	2.00	4.76%
Nitrogen, total as N	mg/L	11.00	8.33%
Ortho Phosphate as P	mg/L	0.35	18.60%
Tot. Phosphate as P	mg/L	0.45	50.00%

#### Review of test 3:

Testing with the Nutrient pad verified that a product of this type has the potential to treat both phosphates and nitrogen compounds. It would be ideal if it could be improved or enhanced to offer more treatment ability/capacity. For the two tests reductions were: Tot Phosphate 61%; Ortho Phosphates 57%; Tot Kjeldahl 16%; Nitrate 31%; Nitrogen 25%. (Appendix G for data)

#### 4. <u>Site 2 (2007):</u>

Testing on nutrients commenced in July of 2007. The cartridge under test contained the new Fabco enhanced Nutrient Pad, FabPhos (FP) that had been under development.

.since 2006. A secondary layer of the CHZ zeolite filter media was also added to the cartridge to aid in Nitrogen compound treatment. (Cartridge designated FPCHZ)

Testing verified good reductions on phosphorous with Total phosphorous (TP) being reduced an average 62% and Ortho-phosphates reduced 40%. Performance on Orthophosphate was a little less than the previous tests using the IC compound but over all effectiveness was good.

The reductions for nitrogen compounds although better than the first test with the CHZ granular media again were less than expected.

One aspect that affected the nitrogen results was the very rural, heavily wooded nature of the site. Unlike Site 3, Site 2 has virtually no landscaped lawns or properties on its perimeter. As a result, soluble nitrates, commonly found in commercial fertilizers were undetectable in 3 out of 4 samples resulting in zero percent reductions being included in the average.

Reductions on Total Kjeldahl and Total nitrogen were an unexceptional 16.7% and 2.5% respectively. Data for Nitrates was inconclusive.

#### Review of Test 4:

The 3<sup>rd</sup> set of samples with an iron enriched filter media demonstrated that this media is capable of effectively reducing Phosphate levels by greater than 40%. The FabPhos has more capacity than the NP and performed as well as the IC media. Therefore, additional testing by Fabco would be focused on the optimization of the FabPhos media.

For Nitrogen compounds, testing of the CHZ zeolite media had demonstrated that effectiveness could vary greatly from sample set to sample set. One theory from a microbiologist suggested that natural bacteria captured in the granular media bed would continue to thrive inside the cartridge, using entrapped organic material for food. This continued growth between rain events would result in an increase of nitrate and Total nitrogen levels stored within the media. As a result first flush samples of the treated effluent could have nitrogen concentrations significantly higher than the raw untreated samples.

To test this theory additional field trials outside the scope of this report, using a cartridge of mainly CHZ zeolite, were completed. In these tests, a new cartridge performed well but subsequent testing over a twenty day period, showed as predicted, substantial increases in both Nitrates and Total Nitrogen. The collected data supports the theory that using granular zeolite media may actually promote the growth of bacteria. As a result CHZ was removed from further testing. (Appendix H for data)

#### 5. <u>Site 2 (2007):</u>

Final testing at this site took place in November 2007. In this test we returned to the concept of a single media technology to isolate effectiveness. Based on the previous results the cartridge consisted of the standard antimicrobial treated pre-filter and FabPhos filter media only.

Previous data collected in the first four tests, confirmed the ability of the iron rich FabPhos material to reduce Total Phosphates and Ortho Phosphates by greater than 40%. Its ability on nitrogen compounds was so far untested.

Earlier in these trials the original Nutrient pad had shown some ability to reduce both nitrogen and phosphate concentrations. As a related product with many of the same properties as the NP media, this testing implied the FabPhos material by itself may be effective on Nitrogen compounds.

To reduce the possibility of bacterial action within the cartridge, the FabPhos material was also treated with our proprietary antimicrobial solution.

Review of test 5:

Table 2: Tests	results at	Site 3 -	2007
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Site 3		IN	OUT	% Change
Tot. Kjeldahl N.	mg/L	3.80	2.40	36.84%
Nitrate as N	mg/L	1.40	0.49	65.00%
Nitrogen, total as N	mg/L	5.20	2.90	44.23%
Ortho Phosphate as P	mg/L	0.58	0.17	70.69%
Tot. Phosphate as P	mg/L	0.57	0.34	40.35%
Site 3		IN	OUT	% Change
Tot. Kjeldahl N.	mg/L	0.80	0.60	25.00%
Nitrate as N	mg/L	0.49	0.49	0.00%
Nitrogen, total as N	mg/L	0.80	0.60	25.00%
Ortho Phosphate as P	mg/L	0.49	0.09	81.63%
Tot. Phosphate as P	mg/L	0.33	0.09	72.73%
Site 3		IN	OUT	% Change
Tot. Kjeldahl N.	mg/L	3.00	1.00	66.67%
Nitrate as N	mg/L	1.00	0.50	50.00%
Nitrogen, total as N	mg/L	4.00	1.50	62.50%
Ortho Phosphate as P	mg/L	1.90	0.26	86.32%
Tot. Phosphate as P	mg/L	2.10	0.30	85.71%

In average the data shows excellent reductions for each of the 4 chemicals

Tot. Kjeldahl N.	Reduced	42.84%
Nitrate as N	Reduced	38.33%
Nitrogen, total as N	Reduced	43.91%
Ortho Phosphate as P	Reduced	79.55%
Tot. Phosphate as P	Reduced	66.26%

These tests demonstrate that the FabPhos material far exceeded the 40% TP reduction required by New York State. And, more importantly the soluble phosphate, which is directly available for plant growth, is reduced by nearly 80%.

Nitrogen levels of all types were also reduced an average of nearly 40%. This data confirms the initial test data obtained in 2006 at Site 3, where the nutrient pad by itself, was very effective on Nitrogen compounds.

Starting with the technology of the Nutrients pad, the iron infused FabPhos offers better performance on phosphates while still treating nitrogen compounds effectively.

The antimicrobial treatment will continue to maintain effectiveness of the filter media by reducing the growth of bacteria and slimes within the cartridge, improving the longevity and service cycle. (Appendix I) (Appendix J summary of all results)

### **Conclusion**

Under the terms of the contract a total of ten (10) StormBasin or StormPod units were installed at designated locations within the town. Fabco Industries was contracted to install, maintain/service and provide testing at three sites. Testing was broken up into two phases: 1) Effectiveness on pathogens/bacteria and 2) treatment of nutrients: phosphorous and nitrogen.

In the first half of the testing program "Beach/Harbor stormwater test program" StormBasin effectiveness was measured using 3 common bacteria indicator organism: E.coli, Fecal Coliform and Enterococcus. This study completed in 2006 is available on the Fabco website www.fabco-industries.com. This report focuses on Test Phase 2: Nutrient treatment and reductions.

#### Testing for effectiveness on nutrients:

3 sites in the Town were designated for evaluation:

- Site 1: a popular and busy town beach
- Site 2: another popular beach with different terrain and environmental conditions than Site 1
- Site 3: a small, affluent community with highly landscaped and maintained yards located near a sensitive waterway.

Testing process: 5 independent tests were run at the 3 sites; each test lasted about one (1) month in duration

Site 1 – Base line nutrient levels only

Site 2 – filtering effectiveness using 1 filter configuration

Site 3: 3 tests - evaluating filtering effectiveness with 3 types of filter media

A total of 13 sets of influent and effluent samples were collected and analyzed by:

Ecotest Laboratories, Inc. 377 Sheffield Ave North Babylon, NY 11703 Tel: 631/422-5777

Baseline concentrations at each site:

Analysis of untreated raw samples from all three sites confirmed that nutrient values in nearly every case, exceeded the National Median Concentrations as indicated in Chapter 2, pg 2-3 in the New York State Stormwater design manual.

Table 3: Nutrient concentrations at test sites (Appendix K baseline values)

	mg/l	Nat'l Median	Site 1	% > median	Site 3	% > median	Site 2	% > median
Tot. Kjeldahl N.		1.47	7.40	403%	5.73	290%	4.60	212.93%
Nitrate as N		0.53	1.15	117%	1.06	100%	0.50	-5.66%
Nitrogen, total as N		2.00	8.55	328%	6.67	233%	4.60	130.00%
Ortho Phosphate as P		0.10	0.03	-75%	0.94	836%	0.50	400.00%
Tot. Phosphate as P		0.26	0.16	-40%	1.22	369%	0.78	200.00%

(Appendix L National Median Concentrations, NYS Stormwater Manual)

### StormBasin and StormPod effectiveness

Based on the raw nutrient analysis, the majority of the sampling was performed at Site 3. This site provided the second highest nitrogen levels and the highest measured phosphorous concentrations in the study.

All samples were first flush samples which typically contain the highest levels of contamination during a single storm event.

3 tests were run at the Site 3 location. A total of 3 cartridge types were evaluated.

The final cartridge featured Fabco's new proprietary filtering media FabPhos-AM. In November 2007, the StormPod unit installed on the site reduced Total nitrogen compounds by over 40% and Total Phosphorous compounds by over 66%

Average of 3 events	Units	Unfiltered	Filtered	% Reduction	Nat'l Median
Tot. Kjeldahl N.	mg/l	2.53	1.33	42.84%	1.47
Nitrate as N		0.96	0.49	38.33%	0.53
Nitrogen, total as N		3.33	1.67	43.91%	2.00
Ortho Phosphate as P		0.99	0.17	79.55%	0.10
Tot. Phosphate as P		1.00	0.24	66.26%	0.26

#### Table 4 Final results:

The results show that the Fabco Industries StormBasin and FabPhos-AM reduced nutrients in stormwater flowing from fertilized, landscaped properties down below the median national average. <u>The 66% reduction in Total Phosphorous comfortably</u> exceeds typical State requirements of 40%.

It is important to realize that these reductions do not include the nutrients attached to sediments and bound to organic matter that are captured and stored in the StormBasin/StormPod collection tub. Maintenance records show over 750 pound of trash, debris and sediments being removed from the site 1 unit annually. With Site 2 contributing over 1100lbs. 100 similar installed units would collect between 37.5 and 55 tons of sediments annually.

#### Nutrient contributions from Sediments and Organic matter:

A coarse analysis of the debris captured at Site 3 showed approximately 150 pounds of trash and debris along with 950 pounds of sediments.

The trash component contained mostly leaves, twigs and grass. In his Nov 2007 article (Stormwater, Nov/Dec 2007, Vol. 8, No. 8, Stormwater pollution: Getting at the Source) L.A Baker estimates a single Maple leaf would contribute 0.3 kilograms of phosphorous per year and that a tree lined road could have greater input than lawns. Capturing and retaining this organic material relatively dry in the StormBasin will significantly reduce the availability of these stored nutrients to the environment. To further aid effectiveness, maintenance activities should be coordinated to clean out the units in the fall months.

Due to the quantity of sediment collected Fabco investigated the size distribution and chemical composition of the load both of which are reported.

Sediment reductions are mandated by most states including New York and for good reason. Many studies have identified nearly every type of pollutant attached to the particles including nutrients.

In our study, Fabco Industries evaluated typical sediments collected in StormBasins located in two Long Island communities

Time period 3-4 mo	Location 1	Location 2
Sediments	120.65 Kg	70.3 Kg
Tot. Kjeldahl	590 mg/Kg	780 mg/Kg
Nitrate	8.2 mg/Kg	< 1.0 mg/Kg
Nitrogen	600 mg/Kg	780 mg/Kg
Tot Phosphate	200 mg/Kg	180 mg/Kg

Table 5: Analysis of sediments collected in Fabco StormBasins

Using the total weights and concentrations indicated in the chart above, the total amounts of nitrogen and phosphorous retained in the captured sediment is shown below.

Location	Total Nitrogen/Total Phoshorous	Yearly (3 cleanout)		
1	2.55 / 0.85oz	7.65 / 2.55oz		
2	1.93 / 0.45oz	5.79 / 1.35oz		

Using the average of these two sites (6.72 TN / 1.95 TP) if we had 100 units the amount of nutrients stored in the captured sediments (yearly) would be equal to 42 pounds of nitrogen and 12 pounds of phosphorous. The State Environmental Resource center (www.serconline.org) suggests that one pound of phosphorous can result in the growth of 350-700 pounds of green algae. 12 pounds would grow 2  $\frac{1}{2}$  to 4  $\frac{1}{2}$  tons of algae.

Again, the nutrient reductions reported earlier reflect reductions in the water samples only and do not include these substantial amounts collected in the debris and in this sediment load.

#### **Recommendations:**

As part of a series of simple Best Management Practices the StormBasin can assist the stormwater manager in complying with State and Federal water quality goals in terms of nutrient reductions.

- 1) StormBasins can be installed quickly at impacted sites using existing drains without additional construction costs. (As an added benefit, pre-installation site surveys can be used to inspect for illicit dumping activities which is also a suggested Stormwater BMP).
- 2) The StormBasin can help meet State Stormwater and Federal TMDL regulations by reducing nutrients using three methods:
  - a. Capturing sediments which can contain many pollutants including nutrients.
  - b. Treating the important soluble nutrient compounds including the Orthophosphates, which are immediately available to plant growth and have potentially the biggest impact on waterways.

- c. Retaining organic debris, keeping it dry and available for easy cleanout before decomposition, and subsequent release of stored nutrients
- 3) The StormBasin will improve existing street sweeping and spill prevention programs by treating the soluble pollutants and capturing sediments and debris that collect or are deposited between scheduled sweeping.

The sweeping program would also keep the StormBasin cleaner, maintaining effectiveness and reducing the maintenance frequency. And in terms of servicing, many new sweepers are equipped with catch basin cleaning attachments that can quickly service the units. This eliminates additional staffing and equipment.

Used as a total solution, spill prevention, sweeping and StormBasin inserts, would keep the paved areas cleaner, minimize the pollutants loads available to first flush action, and reduce the pollutants entering waterways either through the drains or directly from sheet flow off surrounding surfaces.



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